



1 **Simulation characteristics of seismic translation and rotation**
2 **under the assumption of nonlinear small deformation**

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11

12 **Abstract** The conventional theory of elastic-wave propagation is based on classical
13 elastodynamics, assuming linear small deformations of particles. However, recent
14 observations of seismic rotation have revealed significant disparities between actual
15 rotational motions induced by earthquakes in focal areas and near fields compared to
16 theoretical calculations and simulations. Considering the nonlinearity may be the
17 main cause of the discrepancies and based on classical elastodynamic principle, we
18 derive seismic elastic-wave equations with Green strain tensor without the linear
19 small deformation assumption, a different way from using complex nonlinear
20 constitutive relation and try to interpret the mechanism of seismic rotation. By
21 simulating and analyzing translational and rotational components subjected to the
22 three basic and typical vibrating sources, namely, isotropic (ISO), double couple (DC),



23 and compensated linear vector dipole (CLVD), represented by moment tensors, we
24 investigate the wavefield differences between elastic-wave equations based on linear
25 and nonlinear geometric relations and quantify the differences in homogeneous elastic
26 full-space model. Subsequently, we simulate two observed six-component Taiwan
27 earthquakes and compare their differences caused by nonlinear simulations. The
28 results indicate that linear approximation errors are more pronounced in seismic ISO
29 and CLVD sources. And the nonlinearity of small deformation has a more pronounced
30 effect on rotational motions deduced by strong earthquakes. Also, the nonlinear
31 mechanics of seismic rotation can attribute to the complex propagation paths and
32 source mechanisms simultaneously.
33



34 **1 Introduction**

35 Seismic rotational motions are recorded in plenty of earthquakes, especially in
36 strong shocks (Grayzer, 1991; Graizer, 2010; Zhou et al., 2019). Several studies have
37 concluded that rotational motions cannot be neglected in shallow foci and near-field
38 seismology (Kozak, 2009; Sun et al., 2017). In architecture engineering, rotational
39 torsions are encouraged to be considered in assessing the stability of ground motions
40 and building design (Li, 1991; Li and Sun, 2001; Yan, 2017; Huras et al., 2021).
41 Many studies suggest that including seismic rotation data, which records spatial
42 gradients, will enhance the precision of earthquake source prediction and moment
43 tensor inversion (Bernauer et al., 2014; Donner, 2016; Ichinose et al., 2021), as
44 validated in simulations by Hua and Zhang (2002).

45 Lee (2007) ever summarized the practical applications of observing seismic
46 rotations in engineering, attributing seismic rotation to nonlinear elasticity and site
47 effects. Notably, observed rotations during strong ground motions exceed calculated
48 translational components by one to two orders of magnitude. Recognizing the pivotal
49 role of nonlinear wave propagation in addressing geophysical complexities stemming
50 from Earth's heterogeneities, various analytical solutions of nonlinear wave equations
51 have been advanced through iterative techniques based on Green's function (McCall,
52 1994), including the flux-corrected transport method (Yang et al., 2002; Zheng et al.,
53 2006), and perturbation approaches (Bataille and Contreras, 2009; Jia et al., 2020) to
54 investigate the nonlinear effects on elastic waves. However, existing studies
55 predominantly concentrate on the nonlinear constitutive relations of stress and strain,



56 traditionally assuming linear small deformations (Renaud et al., 2012; Renaud et al.,
57 2013b; TenCate et al., 2016; Feng et al., 2018), scarcely exploring nonlinearity in
58 geometric relationship, which may be a crucial aspect that could better approximate
59 strong rotational motions and near-field seismic conditions.

60 Taiwan, located in an active seismic region where earthquakes have garnered
61 attention for their special rotational characteristics of distinctive strike-slip,
62 particularly evident in the southern and northern areas, has been highlighted by
63 extensive broadband seismic observations and earthquake-physical studies (Yu et al.,
64 1999; Wang and Lv, 2006). Oliveira and Bolt's studies (1989) underscore the
65 significant impact of rotation in near-field observations on the island, and Chen et al.
66 (2014) discovered vertical rotations and frequency spectrum variations between
67 horizontal and vertical rotations in the near zone of earthquakes from 2007 to 2008.
68 These findings incline the importance of rotational studies in unraveling Taiwan's
69 underground structures and geodynamics.

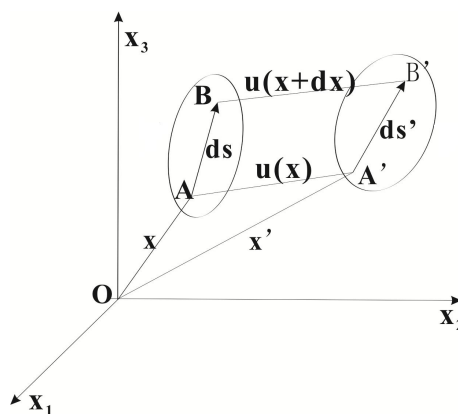
70 In this study, we first investigate the rotational characteristics under the
71 assumption of nonlinear small deformation through numerical simulations of three
72 basic seismic moment tensor sources. Additionally, we engage in theoretical
73 simulations of six-component (6C) wavefields using observations from near and
74 strong seismicity in Taiwan. We employ the Green strain tensor in the simulations of
75 seismic wavefields to discuss the linear approximation and the earthquake
76 mechanisms at play in this region.

77 **2 Theories**



78 2.1 Elastodynamic theory

79 In a three-dimensional orthogonal Cartesian coordinate system depicting an elastic
80 body within an elastic space, illustrated in Fig. 1, consider point **A** within the elastic
81 body, denoted as \mathbf{x} , while point **B**, located in the immediate vicinity of **A**, is indicated
82 as $\mathbf{x}+d\mathbf{x}$. The infinitesimal distance between **A** and **B** is defined as ds . Under
83 instantaneous motivation of an external force, the elastic mass element **AB**
84 experiences displacement $\mathbf{u}(\mathbf{x}, t)$, transitioning to a new position **A'B'**, followed by
85 small deformation of the elastic body, where the positions **A'** and **B'** are designated as
86 \mathbf{x}' and $\mathbf{x}'+d\mathbf{x}'$, respectively, and their distance denoted as ds' . The work done by the
87 external force is primarily transformed into kinetic energy due to displacement and
88 potential energy stemming from elastic deformation. Hence, the change in square of
89 the length of a line element before and after its deformation is used to measure the
90 deformation, i.e., the squared difference in distance between **AB** and **A'B'**, expressed
91 by Eq. (1). The following equations and tensors are written using the Kronecker
92 symbol and dummy indicator rules.



93

94 **Figure 1.** Schematic diagram of displacement and deformation of an elastomer



95 (Adapted from Aki and Richards (2002))

$$96 \quad (ds')^2 - (ds)^2 = \left(\frac{\partial u_j}{\partial x_i} + \frac{\partial u_i}{\partial x_j} + \frac{\partial u_k}{\partial x_i} \cdot \frac{\partial u_k}{\partial x_j} \right) dx_i dx_j, \quad i, j = x, y, z \quad (1)$$

97 Where u_i and u_j denote the displacements in different directions, and x_i and x_j
 98 denote the specific X, Y, and Z axes in Cartesian coordinates. Eq. (2), known as the
 99 Green strain tensor, serves as an objective measure of the strain tensor before and
 100 after the deformation of an elastomer.

$$101 \quad E_{ij} = \frac{1}{2} \left(\frac{\partial u_j}{\partial x_i} + \frac{\partial u_i}{\partial x_j} + \frac{\partial u_k}{\partial x_i} \cdot \frac{\partial u_k}{\partial x_j} \right) \quad (2)$$

102 The strain (e_{ij}) and rotation (r_{ij}) tensors in elastodynamic theory are defined as:

$$103 \quad e_{ji} = \frac{1}{2} \left(\frac{\partial u_j}{\partial x_i} + \frac{\partial u_i}{\partial x_j} \right) \quad (3)$$

$$104 \quad r_{ji} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} - \frac{\partial u_j}{\partial x_i} \right) \quad (4)$$

105 Then, the Green strain tensor can be written as Eq. (5).

$$106 \quad E_{ij} = e_{ij} + \frac{1}{2} e_{ij}^2 + \frac{1}{2} (e_{ij} r_{ij} - r_{ij} e_{ij}) - \frac{1}{2} r_{ij}^2 \quad (5)$$

107 The second-order displacement of nonlinearity in the Green tensor is neglected in
 108 the classical theory of kinetic elasticity. Instead, it focuses solely on the first-order
 109 linear terms, simplifying the nonlinear strain tensor to e_{ij} .

110 In small deformation assumption, the volumetric strain due to shear strain during
 111 elastomer deformation is overlooked, shifting the focus solely to the volumetric strain
 112 along the three principal stress axes (Eq. (6)).

$$113 \quad \theta = \frac{(1 + \theta_{xx})(1 + \theta_{yy})(1 + \theta_{zz}) dxdydz - dxdydz}{dxdydz} \quad (6)$$

$$= e_{xx} + e_{yy} + e_{zz} + e_{xx}e_{yy} + e_{xx}e_{zz} + e_{yy}e_{zz} + e_{xx}e_{yy}e_{zz}$$



114 The simplified linear strain tensor e_{ij} , which ignores the actual nonlinear
 115 displacement term in the Green strain tensor, retains only first-order linear terms in its
 116 volumetric strain (Eq. (7)).

$$117 \quad \theta_e \approx e_{xx} + e_{yy} + e_{zz} = \frac{\partial u_x}{\partial x} + \frac{\partial u_y}{\partial y} + \frac{\partial u_z}{\partial z} \quad (7)$$

118 The linear strain tensor, e_{ij} , disregards the nonlinearity present in the Green strain
 119 tensor, and it becomes evident that only the first-order linear terms are retained in the
 120 volumetric strain (Eq. (7)). The volumetric strain related to the Green strain tensor
 121 features nonlinear second-order displacement terms while discounting higher-order
 122 components (Eq. (8)).

$$123 \quad \theta_E \approx E_{xx} + E_{yy} + E_{zz} + E_{xx}E_{yy} + E_{xx}E_{zz} + E_{zz}E_{yy} \approx \frac{\partial u_x}{\partial x} + \frac{\partial u_y}{\partial y} + \frac{\partial u_z}{\partial z} + \frac{\partial u_x}{\partial x} \frac{\partial u_y}{\partial y} + \frac{\partial u_x}{\partial x} \frac{\partial u_z}{\partial z} + \frac{\partial u_y}{\partial y} \frac{\partial u_z}{\partial z} \quad (8)$$

$$+ \frac{1}{2} \left(\frac{\partial u_x}{\partial x} \cdot \frac{\partial u_x}{\partial x} + \frac{\partial u_y}{\partial y} \cdot \frac{\partial u_y}{\partial y} + \frac{\partial u_z}{\partial z} \cdot \frac{\partial u_z}{\partial z} + \frac{\partial u_x}{\partial y} \cdot \frac{\partial u_x}{\partial y} + \frac{\partial u_y}{\partial x} \cdot \frac{\partial u_y}{\partial x} + \frac{\partial u_x}{\partial y} \cdot \frac{\partial u_y}{\partial x} + \frac{\partial u_x}{\partial z} \cdot \frac{\partial u_x}{\partial z} + \frac{\partial u_z}{\partial x} \cdot \frac{\partial u_x}{\partial z} + \frac{\partial u_x}{\partial z} \cdot \frac{\partial u_z}{\partial x} + \frac{\partial u_y}{\partial z} \cdot \frac{\partial u_y}{\partial z} + \frac{\partial u_z}{\partial y} \cdot \frac{\partial u_y}{\partial z} + \frac{\partial u_y}{\partial z} \cdot \frac{\partial u_z}{\partial y} \right)$$

124 By combining e_{ij} , called the geometric equation, with the linear elastic constitutive
 125 equation given by Hooke and Cauchy equations, the conventional elastic-wave Navier
 126 equation (Eq. (9)) is obtained, which represents the linear elastic-wave equation
 127 within the realm of isotropic media, premised on the assumption of linear small
 128 deformations.

$$129 \quad \rho \frac{\partial^2 u_i}{\partial t^2} = \rho f_i + (\lambda + \mu) \frac{\partial \theta}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j \partial x_j} \quad (9)$$

130 Where ρ symbolizes the density, t denotes the time, f_i denotes the body force, and
 131 λ alongside μ represents the Lamé coefficients. In the nonlinear small deformation
 132 scenario, substituting the Green strain tensor and its corresponding volumetric strain
 133 into constitutive equation and equations of motion, culminating in the formulation of



134 the subsequent equation:

$$\begin{aligned} \rho \frac{\partial^2 u_i}{\partial t^2} = & \rho f_i + (\lambda + \mu) \frac{\partial \theta}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j \partial x_j} \\ & + \lambda \left[\frac{\partial^2 u_k}{\partial x_i \partial x_j} \frac{\partial u_k}{\partial x_j} + \frac{\partial}{\partial x_i} \left(\frac{\partial u_x}{\partial x_x} \frac{\partial u_y}{\partial x_y} + \frac{\partial u_x}{\partial x_x} \frac{\partial u_z}{\partial x_z} + \frac{\partial u_y}{\partial x_y} \frac{\partial u_z}{\partial x_z} \right) \right] + \mu \left(\frac{\partial^2 u_k}{\partial x_i \partial x_j} \frac{\partial u_k}{\partial x_j} + \frac{\partial^2 u_k}{\partial x_j \partial x_i} \frac{\partial u_k}{\partial x_i} \right) \end{aligned} \quad (10)$$

136 Eq. (10) introduces several third-order terms diverging from the composition of
137 Eq. (9). Their difference unveils the nonlinearity in terms of the displacement field \mathbf{u}
138 and the elastic parameters (μ and λ) under nonlinear small deformation. Eq. (10)
139 exhibits more complexity, signifying the introduction of additional physical intricacies
140 into an elastomer's deformation dynamics. The inclusion of nonlinear terms describes
141 the nonlinear response of the medium by linking it with the shear modulus (μ) and the
142 bulk modulus (λ), thereby impacting the propagation attributes of elastic waves. The
143 increment of the equation associated with the shear modulus μ engenders nonlinear
144 effects via the strain tensor, while the increment associated with the bulk modulus λ
145 induces nonlinear effects through the volumetric strain.

146 The disparity between the two wave equations does not directly translate to the
147 final displacement field discrepancies. The displacement field in Eq. (10) is the result
148 of the nonlinear small deformation, in contrast to Eq. (9), where such nonlinear effects
149 are absent. Therefore, the velocity-stress equations using the Green strain tensor are
150 derived next to compare the difference in wave fields between the two by numerical
151 simulation of seismic wavefields.

152

153 2.2 Velocity-stress elastic wave equations

154 The staggered-grid finite-difference method is well-established for performing



155 numerical simulations of seismic wavefields. By discretizing the medium and the
 156 wave equations, the numerical solution of the wavefield is obtained at each grid point
 157 under each time node as time progresses. In general, the first-order velocity-stress
 158 elastic wave equations under the assumption of linear small deformation in
 159 3-dimensional (3D) isotropic media are

$$\begin{cases}
 \frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \sigma_{xy}}{\partial y} + \frac{\partial \sigma_{xz}}{\partial z} + f_x = \rho \frac{\partial v_x}{\partial t} \\
 \frac{\partial \sigma_{yx}}{\partial x} + \frac{\partial \sigma_{yy}}{\partial y} + \frac{\partial \sigma_{yz}}{\partial z} + f_y = \rho \frac{\partial v_y}{\partial t} \\
 \frac{\partial \sigma_{zx}}{\partial x} + \frac{\partial \sigma_{zy}}{\partial y} + \frac{\partial \sigma_{zz}}{\partial z} + f_z = \rho \frac{\partial v_z}{\partial t} \\
 \frac{\partial \sigma_{xx}}{\partial t} = (\lambda + 2\mu) \frac{\partial v_x}{\partial x} + \lambda \frac{\partial v_y}{\partial y} + \lambda \frac{\partial v_z}{\partial z} \\
 \frac{\partial \sigma_{yy}}{\partial t} = \lambda \frac{\partial v_x}{\partial x} + (\lambda + 2\mu) \frac{\partial v_y}{\partial y} + \lambda \frac{\partial v_z}{\partial z} \\
 \frac{\partial \sigma_{zz}}{\partial t} = \lambda \frac{\partial v_x}{\partial x} + \lambda \frac{\partial v_y}{\partial y} + (\lambda + 2\mu) \frac{\partial v_z}{\partial z} \\
 \frac{\partial \sigma_{xy}}{\partial t} = \mu \left(\frac{\partial v_y}{\partial x} + \frac{\partial v_x}{\partial y} \right) \\
 \frac{\partial \sigma_{xz}}{\partial t} = \mu \left(\frac{\partial v_z}{\partial x} + \frac{\partial v_x}{\partial z} \right) \\
 \frac{\partial \sigma_{yz}}{\partial t} = \mu \left(\frac{\partial v_z}{\partial y} + \frac{\partial v_y}{\partial z} \right) \\
 R_x = \frac{1}{2} \left(\frac{\partial v_z}{\partial y} - \frac{\partial v_y}{\partial z} \right) \\
 R_y = \frac{1}{2} \left(\frac{\partial v_x}{\partial z} - \frac{\partial v_z}{\partial x} \right) \\
 R_z = \frac{1}{2} \left(\frac{\partial v_y}{\partial x} - \frac{\partial v_x}{\partial y} \right)
 \end{cases} \quad (11)$$

161 Where σ_{ji} denotes the stress tensor, v_x , v_y , and v_z denote the velocity of X, Y, and Z
 162 components. \mathbf{R}_{xz} corresponds to the rotation rate around Y axis, commonly referred to
 163 as \mathbf{R}_Y in rotational seismology, as well as \mathbf{R}_X and \mathbf{R}_Z .

164 Similarly, the velocity-stress elastic wave equations under the assumption of
 165 nonlinear small deformation in 3D isotropic media can be given as Eq. (12).



$$\begin{cases}
 \frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \sigma_{yy}}{\partial y} + \frac{\partial \sigma_{zz}}{\partial z} + f_x = \rho \frac{\partial v_x}{\partial t} \\
 \frac{\partial \sigma_{yx}}{\partial x} + \frac{\partial \sigma_{yy}}{\partial y} + \frac{\partial \sigma_{yz}}{\partial z} + f_y = \rho \frac{\partial v_y}{\partial t} \\
 \frac{\partial \sigma_{zx}}{\partial x} + \frac{\partial \sigma_{zy}}{\partial y} + \frac{\partial \sigma_{zz}}{\partial z} + f_z = \rho \frac{\partial v_z}{\partial t}
 \end{cases}$$

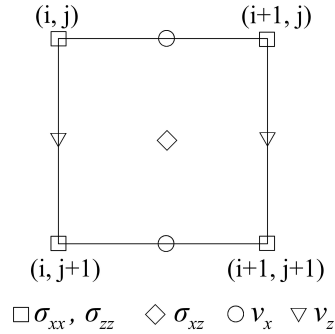
$$\begin{cases}
 \frac{\partial \sigma_{xx}}{\partial t} = (\lambda + 2\mu) \frac{\partial v_x}{\partial x} + \lambda \frac{\partial v_y}{\partial y} + \lambda \frac{\partial v_z}{\partial z} + 2 dt \lambda \cdot \left(\frac{\partial v_x}{\partial x} \frac{\partial v_y}{\partial y} + \frac{\partial v_x}{\partial x} \frac{\partial v_z}{\partial z} + \frac{\partial v_y}{\partial y} \frac{\partial v_z}{\partial z} \right) + dt (\lambda + 2\mu) \cdot \left(\frac{\partial v_x}{\partial x} \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} \frac{\partial v_y}{\partial y} + \frac{\partial v_z}{\partial z} \frac{\partial v_z}{\partial z} \right) \\
 + dt \cdot \lambda \cdot \left(\frac{\partial v_x}{\partial y} \frac{\partial v_x}{\partial y} + \frac{\partial v_x}{\partial y} \frac{\partial v_y}{\partial y} + \frac{\partial v_x}{\partial y} \frac{\partial v_z}{\partial z} \right) + dt \cdot \lambda \cdot \left(\frac{\partial v_x}{\partial z} \frac{\partial v_x}{\partial z} + \frac{\partial v_y}{\partial z} \frac{\partial v_y}{\partial z} + \frac{\partial v_z}{\partial z} \frac{\partial v_z}{\partial z} \right) \\
 \frac{\partial \sigma_{yy}}{\partial t} = \lambda \frac{\partial v_x}{\partial x} + (\lambda + 2\mu) \frac{\partial v_y}{\partial y} + \lambda \frac{\partial v_z}{\partial z} + 2 dt \lambda \cdot \left(\frac{\partial v_x}{\partial x} \frac{\partial v_y}{\partial y} + \frac{\partial v_x}{\partial x} \frac{\partial v_z}{\partial z} + \frac{\partial v_y}{\partial y} \frac{\partial v_z}{\partial z} \right) + dt \lambda \cdot \left(\frac{\partial v_x}{\partial x} \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} \frac{\partial v_y}{\partial y} + \frac{\partial v_z}{\partial z} \frac{\partial v_z}{\partial z} \right) \\
 + dt \cdot (\lambda + 2\mu) \cdot \left(\frac{\partial v_x}{\partial y} \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial y} \frac{\partial v_y}{\partial y} + \frac{\partial v_z}{\partial y} \frac{\partial v_z}{\partial y} \right) + dt \cdot \lambda \cdot \left(\frac{\partial v_x}{\partial z} \frac{\partial v_x}{\partial z} + \frac{\partial v_y}{\partial z} \frac{\partial v_y}{\partial z} + \frac{\partial v_z}{\partial z} \frac{\partial v_z}{\partial z} \right) \\
 \frac{\partial \sigma_{zz}}{\partial t} = \lambda \frac{\partial v_x}{\partial x} + \lambda \frac{\partial v_y}{\partial y} + (\lambda + 2\mu) \frac{\partial v_z}{\partial z} + 2 dt \lambda \cdot \left(\frac{\partial v_x}{\partial x} \frac{\partial v_y}{\partial y} + \frac{\partial v_x}{\partial x} \frac{\partial v_z}{\partial z} + \frac{\partial v_y}{\partial y} \frac{\partial v_z}{\partial z} \right) + dt \lambda \cdot \left(\frac{\partial v_x}{\partial x} \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} \frac{\partial v_y}{\partial y} + \frac{\partial v_z}{\partial z} \frac{\partial v_z}{\partial z} \right) \\
 + dt \cdot \lambda \cdot \left(\frac{\partial v_x}{\partial y} \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial y} \frac{\partial v_y}{\partial y} + \frac{\partial v_z}{\partial y} \frac{\partial v_z}{\partial y} \right) + dt \cdot (\lambda + 2\mu) \cdot \left(\frac{\partial v_x}{\partial z} \frac{\partial v_x}{\partial z} + \frac{\partial v_y}{\partial z} \frac{\partial v_y}{\partial z} + \frac{\partial v_z}{\partial z} \frac{\partial v_z}{\partial z} \right) \\
 \frac{\partial \sigma_{xy}}{\partial t} = \mu \left(\frac{\partial v_x}{\partial x} + \frac{\partial v_x}{\partial y} \right) + dt \cdot 2\mu \cdot \left(\frac{\partial v_x}{\partial x} \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x} \frac{\partial v_y}{\partial y} + \frac{\partial v_z}{\partial x} \frac{\partial v_z}{\partial y} \right) \\
 \frac{\partial \sigma_{yz}}{\partial t} = \mu \left(\frac{\partial v_y}{\partial z} + \frac{\partial v_z}{\partial x} \right) + dt \cdot 2\mu \cdot \left(\frac{\partial v_x}{\partial z} \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial z} \frac{\partial v_y}{\partial x} + \frac{\partial v_z}{\partial z} \frac{\partial v_z}{\partial x} \right) \\
 \frac{\partial \sigma_{zx}}{\partial t} = \mu \left(\frac{\partial v_z}{\partial y} + \frac{\partial v_y}{\partial z} \right) + dt \cdot 2\mu \cdot \left(\frac{\partial v_x}{\partial y} \frac{\partial v_x}{\partial z} + \frac{\partial v_y}{\partial y} \frac{\partial v_y}{\partial z} + \frac{\partial v_z}{\partial y} \frac{\partial v_z}{\partial z} \right) \\
 \begin{cases}
 R_x = \frac{1}{2} \left(\frac{\partial v_z}{\partial y} - \frac{\partial v_y}{\partial z} \right) \\
 R_y = \frac{1}{2} \left(\frac{\partial v_x}{\partial z} - \frac{\partial v_z}{\partial x} \right) \\
 R_z = \frac{1}{2} \left(\frac{\partial v_y}{\partial x} - \frac{\partial v_x}{\partial y} \right)
 \end{cases}
 \end{cases} \quad (12)$$

167 Where the variables and symbols are defined in the same way as in Eq. (11).

168

169 2.3 Staggered-grid finite difference method

170 This study utilizes the staggered-grid finite difference method to simulate the
 171 seismic wavefields (Sun et al., 2018). The model is divided into two sets of grids,
 172 wherein the velocity and stress of the medium are defined in separate grid systems
 173 (Madariaga, 1976). The grid configuration for a two-dimensional model scenario is
 174 illustrated in Fig. 2.



175
 176

Figure 2. Schematic diagram of 2D staggered grids.

177 Based on Eqs. (11) and (12), we can simulate the seismic waves propagating in
 178 discrete grids with two-order time and six-order space differential approximations. To
 179 weaken the boundary reflections, perfectly matched absorbing layer boundary
 180 conditions are adapted to the boundaries (Dong & Ma 2000). Alternatively, the
 181 acoustic boundary replacement method is adopted to ensure the free-surface condition
 182 at the upper boundary (Xu et al., 2007; Wang et al., 2012).

183

184 2.4 Simulation parameters

185 For the physical process of source excitation, when the seismic wavelength under
 186 study substantially surpasses the scale of the involved source, the seismic source can
 187 be regarded as a point source. The seismic moment tensor, represented by equation
 188 (13), is the most comprehensive depiction of seismic point sources.

$$189 \quad \mathbf{M} = \begin{pmatrix} M_{xx} & M_{xy} & M_{xz} \\ M_{yx} & M_{yy} & M_{yz} \\ M_{zx} & M_{zy} & M_{zz} \end{pmatrix}, i, j = x, y, z \quad (13)$$

190 In Eq. (11), M_{ij} represents each moment-element component. The first index
 191 signifies the force direction, and the second index signifies the direction of force arm.



192 The moment tensor can be decomposed into three distinct parts: the isotropy
193 component (ISO), the double couple component (DC), and the compensated linear
194 vector dipole component (CLVD) (Knopoff and Randall, 1970). The ISO component
195 represents the volume expansion of the focal area, characterized by a non-zero trace
196 and uniform force and direction of force arm in three vector dipoles. The DC
197 component denotes the dislocation of the two fault walls without volume variation.
198 The CLVD component is also composed of three vector dipoles, with one being twice
199 as large as the other two. The three basic seismic source components can be expressed
200 as follows.

$$201 \quad \mathbf{M}^{ISO} = \begin{pmatrix} M_{xx} & 0 & 0 \\ 0 & M_{yy} & 0 \\ 0 & 0 & M_{zz} \end{pmatrix} \quad (14)$$

$$202 \quad \mathbf{M}^{DC} = \begin{pmatrix} 0 & M_{xy} & 0 \\ M_{yx} & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} \quad (15)$$

$$203 \quad \mathbf{M}^{CLVD} = \begin{pmatrix} M_{xx} & 0 & 0 \\ 0 & M_{yy} & 0 \\ 0 & 0 & -2M_{zz} \end{pmatrix} \quad (16)$$

204

205 In numerical simulations, the Ricker wavelet with a central frequency of 0.5 Hz is
206 employed as a seismic source wavelet to simulate the three simplest sources: ISO, DC,
207 and CLVD. The body force, represented by the moment tensor, can be converted into
208 a velocity source by incrementally being added to individual velocity components to
209 simulate the three basic sources (Graves, 1996). The specific loading equations in the
210 grid system are outlined below.



$$211 \quad \text{ISO:} \quad \begin{cases} \Delta v_x^{n+\frac{1}{2}}\left(i+\frac{1}{2}, j, k\right) = \frac{M_{xx} dt}{\rho V dx} f^n \\ \Delta v_x^{n+\frac{1}{2}}\left(i-\frac{1}{2}, j, k\right) = \frac{-M_{xx} dt}{\rho V dx} f^n \\ \Delta v_y^{n+\frac{1}{2}}\left(i, j+\frac{1}{2}, k\right) = \frac{M_{yy} dt}{\rho V dy} f^n \\ \Delta v_y^{n+\frac{1}{2}}\left(i, j-\frac{1}{2}, k\right) = \frac{-M_{yy} dt}{\rho V dy} f^n \\ \Delta v_z^{n+\frac{1}{2}}\left(i, j, k+\frac{1}{2}\right) = \frac{M_{zz} dt}{\rho V dz} f^n \\ \Delta v_z^{n+\frac{1}{2}}\left(i, j, k-\frac{1}{2}\right) = \frac{-M_{zz} dt}{\rho V dz} f^n \end{cases} \quad (17)$$

$$212 \quad \text{DC:} \quad \begin{cases} \Delta v_x^{n+\frac{1}{2}}\left(i+\frac{1}{2}, j, k\right) = \frac{-M_{xy} dt}{\rho V dy} f^n \\ \Delta v_x^{n+\frac{1}{2}}\left(i+\frac{1}{2}, j-1, k\right) = \frac{M_{xy} dt}{\rho V dy} f^n \\ \Delta v_y^{n+\frac{1}{2}}\left(i, j-\frac{1}{2}, k\right) = \frac{M_{yx} dt}{\rho V dx} f^n \\ \Delta v_y^{n+\frac{1}{2}}\left(i+1, j-\frac{1}{2}, k\right) = \frac{-M_{yx} dt}{\rho V dx} f^n \end{cases} \quad (18)$$

$$213 \quad \text{CLVD:} \quad \begin{cases} \Delta v_x^{n+\frac{1}{2}}\left(i+\frac{1}{2}, j, k\right) = \frac{M_{xx} dt}{\rho V dx} f^n \\ \Delta v_x^{n+\frac{1}{2}}\left(i-\frac{1}{2}, j, k\right) = \frac{-M_{xx} dt}{\rho V dx} f^n \\ \Delta v_y^{n+\frac{1}{2}}\left(i, j+\frac{1}{2}, k\right) = \frac{M_{yy} dt}{\rho V dy} f^n \\ \Delta v_y^{n+\frac{1}{2}}\left(i, j-\frac{1}{2}, k\right) = \frac{-M_{yy} dt}{\rho V dy} f^n \\ \Delta v_z^{n+\frac{1}{2}}\left(i, j, k+\frac{1}{2}\right) = \frac{-2M_{zz} dt}{\rho V dz} f^n \\ \Delta v_z^{n+\frac{1}{2}}\left(i, j, k-\frac{1}{2}\right) = \frac{2M_{zz} dt}{\rho V dz} f^n \end{cases} \quad (19)$$

214 Δv denotes the velocity increment; n denotes the time sampling node; dt , ρ , and V
 215 represent the time sampling interval, medium density, and the medium model's unit
 216 volume, respectively. The source-time function f^n denotes the Ricker wavelet's
 217 amplitude at the corresponding time node.



218 To focus on the influence of different small deformation scenarios on seismic
219 elastic waves, we only discuss the characteristics in a 3D isotropic full-space
220 homogeneous medium. The model is set with a size of 60 km (x) \times 60 km (y) \times 60 km
221 (z), with mesh division spacing set at 0.5 km. Model properties include $v_p=4400$ m/s,
222 $v_s=3000$ m/s, and $\rho=2600$ kg/m³. The moment source is positioned at the model's
223 center, where $x=y=z=30$ km. The time sampling interval is 15 ms, and the total
224 recording time spans 10 seconds.

225

226 **3 Wavefield simulations of three types of basic seismic source**

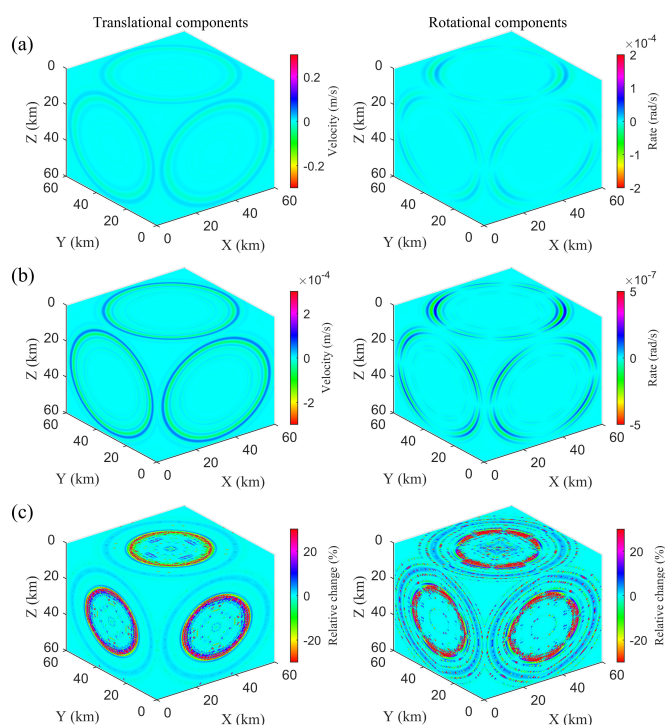
227 3.1 ISO source

228 Under the assumption of nonlinear small deformation related to the condition of
229 the Green strain tensor, the 3-component translational and rotational seismic
230 snapshots are synthesized and illustrated in Fig. 3a. These snapshots demonstrate the
231 generation of solely P-wave, with minimal energy projected in rotational components
232 upon the excitation of ISO source.

233 To highlight the distinction in wave propagation between linear and nonlinear
234 conditions, we present the wavefield difference and their approximation with the
235 relative change in Fig. 3b and c. Minimal disparities are observed in P-wave fronts,
236 indicating that the assumption of linear small deformation is satisfied for P-wave in
237 ISO source simulation. Conversely, examining the S-wave fronts in Fig. 3b and their
238 relative changes (ranging approximately between 5-20 percent) in Fig. 3c lead to the



239 conclusion that even in the ISO simulation, the coupling of P- and S-waves in the
240 wave equations allows the generation of S-waves, a phenomenon that is unattainable
241 under conditions of linear small deformation.



242
243 **Figure 3.** Wavefield comparisons at 8th second excited by ISO source. (a) presents
244 the wavefield snapshots under nonlinear small deformation, (b) presents the
245 difference between linear and nonlinear conditions, and (c) presents their relative
246 change in percentage (using the linear result as the denominator)

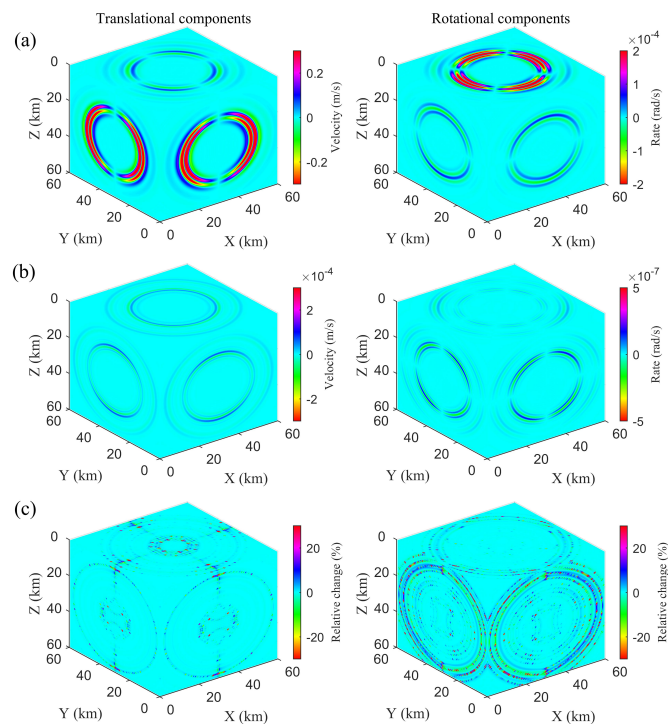
247

248 3.2 DC source

249 The wavefields excited by the DC source are illustrated in Fig. 4a, revealing the
250 generation of relatively weak P and stronger S waves. The application of double force



251 moments (M_{xy} and M_{yx}) loaded within the x-y plane results in the X- and
252 Y-components of translational motions being stronger than the Z-component.
253 Consequently, the \mathbf{R}_Z exhibits a greater degree of wavefield energy than the \mathbf{R}_X and
254 \mathbf{R}_Y components. From the wavefield differences and relative change between the two
255 assumptions (Fig. 4b and c), it becomes evident that the discrepancy in S-wave is
256 notable, and the relative change in P wave is more prominent in the rotational
257 components (below 10 %). Moreover, the distinction in the wavefront polarity of the
258 P- and S-wave in the wavefield caused by nonlinearity is totally different from the
259 polarity of the wavefield itself, as illustrated in Fig. 4a.



260

261 **Figure 4.** Wavefield comparisons at 8th second excited by DC source. (a)

262 presents the wavefield snapshots under nonlinear small deformation, (b) presents the

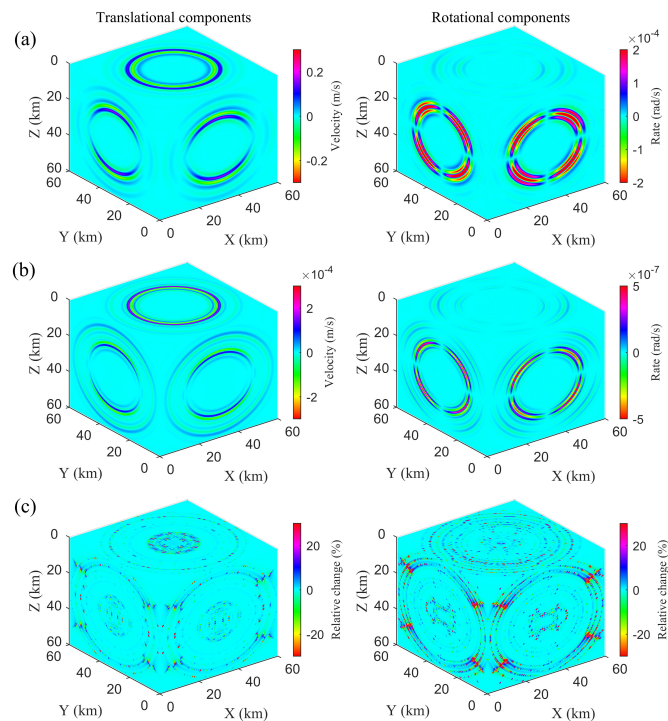


263 difference between the linear and nonlinear conditions, and (c) presents their relative
264 change with percentage (using the linear result as the denominator)

265

266 3.3 CLVD source

267 Fig. 5a displays the results generated by CLVD source. In comparison to the
268 outcomes of ISO and DC sources, the CLVD elicits more pronounced S waves
269 primarily projected in \mathbf{R}_X and \mathbf{R}_Y components. Moreover, the wavefield differences
270 between linearity and nonlinearity intensify, particularly in S wave in rotational
271 motion (Fig. 5b). Their maximum relative change can reach up to 10 percent,
272 especially along the diagonal direction of 45 degrees (Fig. 5c).



273

274 **Figure 5.** Wavefield comparisons at 8th second excited by CLVD source. (a)



275 presents the wavefield snapshots under nonlinear small deformation, (b) presents the
276 difference between the linear and nonlinear conditions, and (c) presents their relative
277 change with percentage (using the linear result as the denominator)

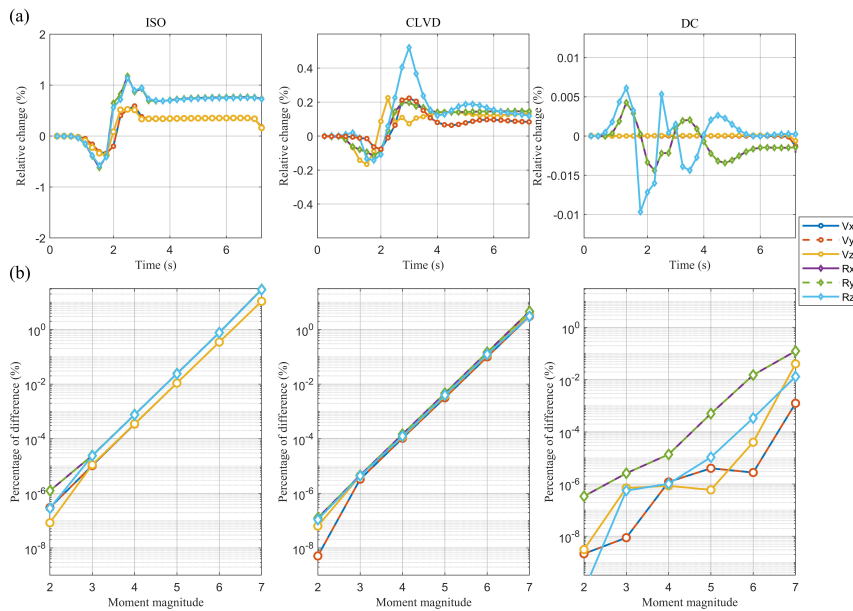
278

279 3.4 Comparisons of wavefield energy for basic seismic sources

280 The disparities in propagation of nonlinear elastic waves in homogeneous media
281 are predominantly observed in rotational components, as evidenced by the
282 aforementioned comparisons and analyses. Further calculating the wavefield energy
283 for the above wavefield snapshot display area and comparing the variations of wave
284 energy in relative changes over time progression and the change at the 8th second
285 with the seismic moment magnitude increasing, as illustrated in Fig. 6. In Fig. 6a, the
286 overall errors in wavefield energy consistently remain below 1 percent as the wave
287 propagates near the source area with small magnitude, signifying that the linear
288 assumption is adequate for the three basic moment tensor sources. In Fig. 6b, the
289 changing curves for the DC source display less smoothness than those for the CLVD,
290 and the relative change in rotational components consistently outweighs this in
291 translational components. Moreover, the curves demonstrate a nearly exponential
292 increase with rising earthquake magnitude. Upon reaching a strong magnitude of 7,
293 especially for the ISO source, the errors in rotational motions reach 25 percent, while
294 these in translation amount to approximately 10 percent. The error due to CLVD
295 sources can also reach about 5 %, while the DC-induced error remains small. Because
296 the DC source component typically dominates the focal mechanisms for the majority



297 of earthquakes, as opposed to the ISO component (Zhao and Zhang, 2022), it can be
298 inferred that the approximation of linear scenario is well-suited for the majority of
299 seismic body waves simulations, except in instances of strong seismic activity.



300

301 **Figure 6.** Relative changes of wavefield energy induced by nonlinearity with (a)

302 spreading time and (b) increasing earthquake magnitude

303

304 4 Seismic observations and simulations of two Taiwan earthquakes

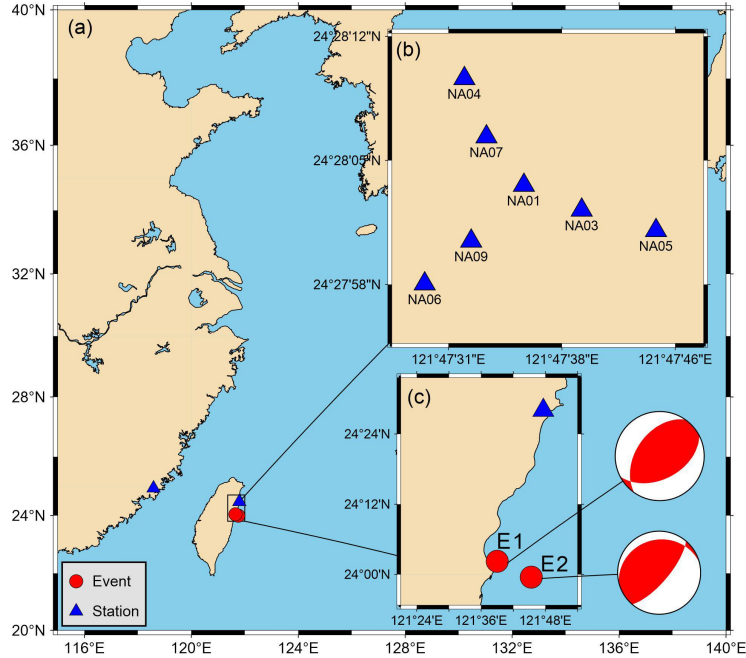
305 4.1 Hualien earthquakes

306 Taiwan, situated at the confluence of three significant tectonic plates - the
307 Philippine Sea Plate, the Eurasia Plate, and the Pacific Ocean Plate, experiences
308 frequent seismic activity, particularly moderate to large earthquakes annually (Zheng
309 et al., 2005). The 2018 Hualien earthquake with a magnitude of M_W 5.41 (referred to



310 as **E1**) and the 2019 Hualien earthquake with a magnitude of M_W 6.13 (referred to as
311 **E2**), with epicenter depths of 15 km and 30 km, respectively, occurred off the eastern
312 coast of Taiwan. The epicenter locations and station placements depicted by GMT are
313 shown in Fig. 7 (Wessel et al., 2019). The receiver for **E2**, located in Fujian province,
314 is positioned 327 km from the epicenter (Fig. 7a). Additionally, a seismic array
315 comprising seven 3C translational seismometers was deployed approximately 53 km
316 from the epicenter of **E1** (Yuan et al., 2020) (Fig. 7b). A blueSeis-3A fiber-optic
317 rotational seismometer was placed at the NA01 station in the center of the array to
318 directly record the seismic rotational rates (Bernauer et al. 2018; Cao et al., 2021).

319 According to the monitoring data from the U.S. Geological Survey (USGS,
320 <https://www.usgs.gov/>), both **E1** and **E2** were triggered by reverse faults, and beach
321 balls representing their focal mechanisms are shown in Fig. 7c. The moment tensor
322 parameters of **E1** and **E2** are presented in Eqs. (20) and (21), respectively.



323

324

Figure 7. Epicenters and observation sites of the two earthquakes

325

326

$$\begin{aligned} M_{rr} &= 9.942 \times 10^{16}, M_{tt} = -7.569 \times 10^{16}, M_{pp} = -2.373 \times 10^{16} \\ M_{rt} &= 7.372 \times 10^{16}, M_{rp} = 1.0965 \times 10^{17}, M_{tp} = -4.156 \times 10^{16} \end{aligned} \quad (20)$$

327

$$\begin{aligned} M_{rr} &= 1.8247 \times 10^{18}, M_{tt} = -1.064 \times 10^{18}, M_{pp} = -7.607 \times 10^{17} \\ M_{rt} &= 3.141 \times 10^{17}, M_{rp} = -3.155 \times 10^{17}, M_{tp} = -1.114 \times 10^{18} \end{aligned} \quad (21)$$

328

329 4.2 Wavefield simulations of the Taiwan earthquakes

330

To simulate **E1** and **E2**, we implement the free-surface condition at the upper

331

surface and absorbing boundary conditions in other directions of the 3D model.

332

According to the CRUST1.0 model (Laske et al., 2013), the subsurface medium at the

333

E1 observation station is divided into five distinct layers, as detailed in Table 1. The

334

3D model is constructed with a size of 60 km (x , NS) \times 20 km (y , EW) \times 30 km (z ,



335 vertical) to suit the specifics of the observation system, with the corresponding
336 parameters shown in Table 2.

337 **Table 1** Underground layered medium at observing stations

Layer	Thickness (km)	Vp (km/s)	Vs (km/s)	ρ (kg/m ³)
1	0.50	2.50	1.07	2.11
2	10.12	5.80	3.40	2.63
3	9.81	6.30	3.62	2.74
4	9.82	6.90	3.94	2.92
5	-	7.70	4.29	3.17

338

339 **Table 2** Parameters for simulating model 1 (E1)

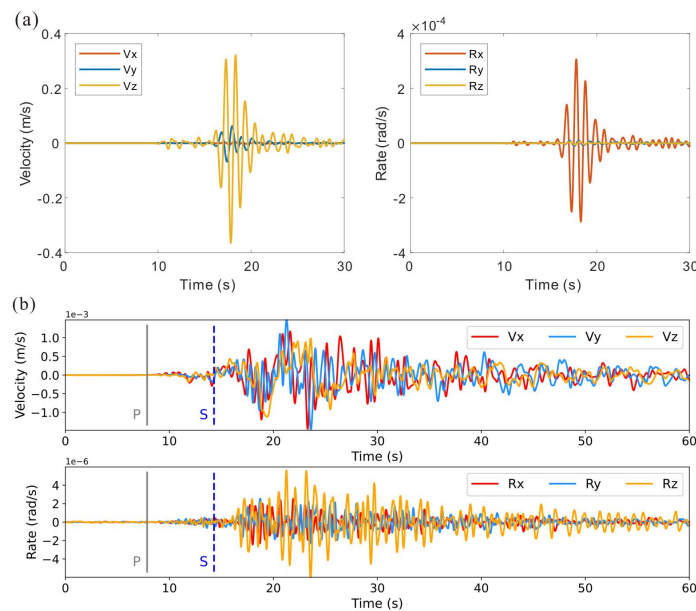
Items	Parameters
Source type	Eq. (20)
Central frequency	1 Hz
Grid interval	1 km
Time interval	5 ms
Source position	(0, 0, 15 km)
Receiver position	(53 km, , 0 km)
Recording time	30 s

340

341 Sorting the synthetic records from model 1 at coordinates X=53 km and Y=4 km,
342 corresponding to the NA01 station, the seismic waveforms are presented in Fig. 8a. It
343 can be found that, apart from direct P- and S-waves, E1 predominantly exhibits
344 elliptical polarization in X-Z vertical plane and rotational movements around Y-axis
345 induced by Rayleigh wave in the north-south vertical plane. The large order of
346 magnitude difference in amplitude between theoretical simulations and actual
347 observations is due to the assumption of elastic media, though the actual propagation
348 media are usually viscoelastic, which will absorb and attenuate seismic energy and
349 high frequency.



350 The unavoidable site effect leads to the practical observation in Fig. 8b displaying
351 significantly stronger horizontal components than vertical ones (Abercrombie, 1997;
352 Guatteri et al., 2001). The site effect and the nearly northeast strike of the seismogenic
353 fault result in pronounced translational components and R_z component recordings
354 mixed with complex seismic waves after P- and S-wave arrivals, indicating the
355 presence of Love waves and significant disparities between the actual Earth's medium
356 and the simplified Crust model. Fig. 8 also shows that the simulated rotational
357 components are 1000 times of magnitude weaker than the simulated translational
358 components, but the observed rotational motions are 250 times weaker than the
359 translational ones.



360
361 **Figure 8.** 6C seismic records of (a) theoretical simulation under linear small
362 deformation for E1. In (b), for the real seismic records, a band-pass filter of 0.1 Hz to
363 2 Hz is applied, and the corresponding arrival times of P and S waves are calculated



364 according to the iasp91 model (Kennett and Engdahl, 1991)

365

366 **Table 3** Parameters for simulating model 2 (**E2**).

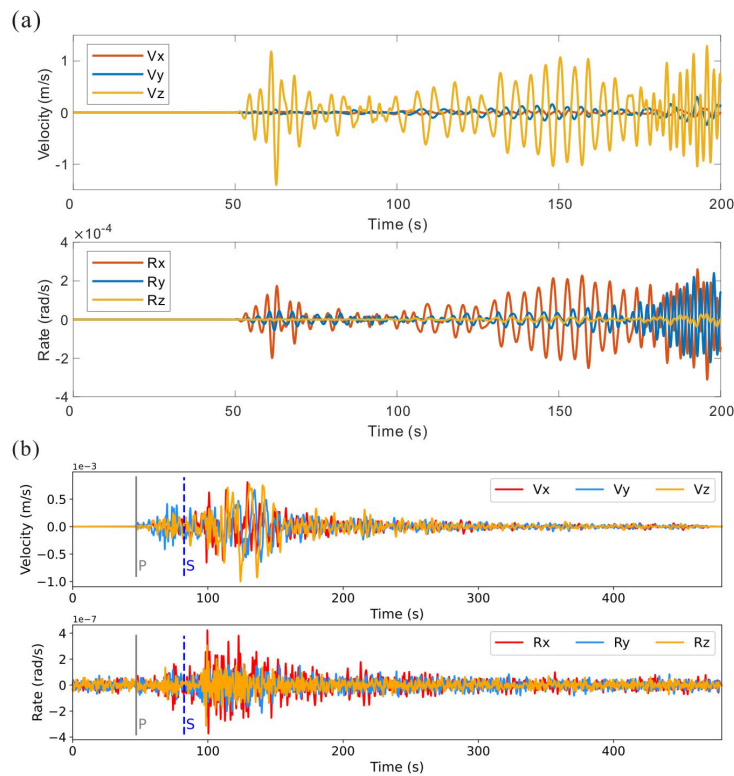
Items	Parameters
Source type	Eq. (21)
Central frequency	0.5 Hz
Grid interval	5 km
Time interval	2 ms
Source position	(0, 310 km, 30 km)
Receiver position	(:, 0 km, 0 km)
Recording time	300 s

367

368 The same modeling approach is adopted to simulate **E2**, with the parameters of
369 model 2 detailed in Table 3, featuring a size of 150 km (x, NS) \times 350 km (y, EW) \times 50
370 km (z, vertical). The 6C seismic recordings at X=100 km and Y=0 km, corresponding
371 to the receiver station, are extracted from the simulation result of model 2, as
372 displayed in Fig. 9a. The simulated records show a dominance of V_Z over V_X and V_Y
373 components, with R_X and R_Y components exhibiting more strength than R_Z
374 component, showcasing the rotational motions primarily occurring in the horizontal
375 direction. In addition to the direct P and S waves and surface waves, this intense
376 seismic shock generated strong secondary waves. In the actual observation records
377 (Fig. 9b), where the station is located on solid rock within a tunnel, the V_Z component
378 is slightly stronger than the V_X and V_Y components, while the R_Z component is
379 slightly weaker than the R_X and R_Y components. This suggests that the rotational
380 motions for **E2** are predominantly in horizontal directions, and the site effect is
381 relatively weaker. In addition, the amplitude difference between the actual observed



382 rotational and translational components is smaller than the amplitude difference
383 between the simulated advective and rotational components, and the observed
384 rotational component is relatively stronger, which is the same as the characteristic
385 shown in Fig. 9. That is consistent with previous studies that have argued that the
386 observed rotational components have a relatively stronger amplitude than the
387 rotational component converted from translational components (Teisseyre et al.,
388 2003).



389

390 **Figure 9.** 6C seismic records of (a) theoretical simulation under linear small
391 deformation for **E2**. In (b), for the real seismic records, a band-pass filter of 0.1 Hz to
392 1 Hz is applied, and the corresponding arrival times of P and S waves are calculated



393 according to the iasp91 model (Kennett and Engdahl, 1991)

394 Following the numerical simulation of **E1** and **E2** under the conditions of linear

395 and nonlinear simulations, respectively, we make a theoretical comparison by

396 calculating the relative differences between the two scenarios. The relative changes in

397 root-mean-square (RMS) amplitude are used to compare the linear errors of these two

398 earthquakes. The RMS amplitude values of the waveforms recorded in a 2-s time

399 window are calculated at 1-s intervals to reflect the energy of the seismic recordings,

400 and then the relative change percentage of RMS amplitude of the nonlinear simulation

401 results relative to that of the linear simulation is derived accordingly, and the results

402 are shown in Fig. 10.

403 In Fig. 10a, it can be seen that the error of the nonlinear simulation of **E1** is very

404 small relative to the linear simulation, and only the error on the V_x component is

405 slightly larger but is less than 0.4 %. This indicates that for the simulation of **E1**, the

406 error introduced by the linear approximation is basically negligible. For the results of

407 **E2** in Fig. 10b, the translational components show larger errors than the rotational

408 components, especially the V_x and V_y components, with errors up to 10 %, and the

409 errors on the V_z components are basically within 5 %; the linear approximation errors

410 on the three rotational components are even smaller, basically within 2 %. For the

411 body waves dominated records before 120 s, R_x and R_y components reflect a larger

412 error percentage than R_z component. In the surface-wave records after the 150 s, the

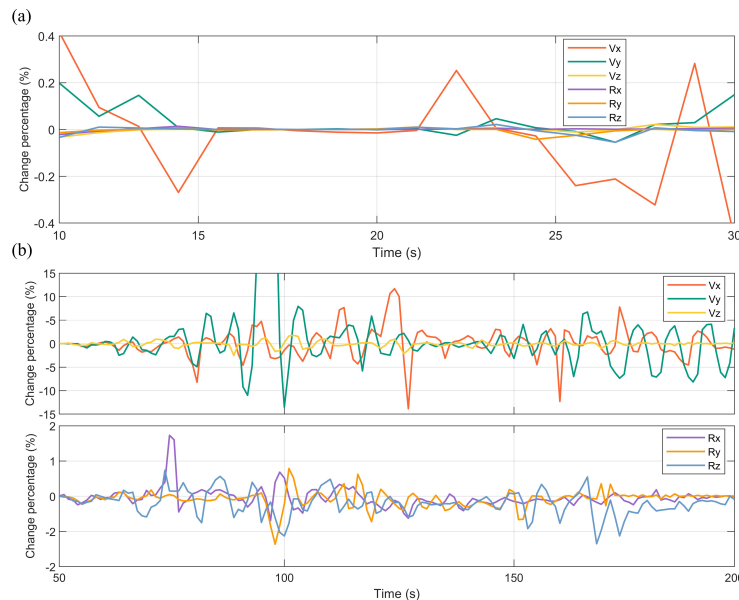
413 R_z component shows increased nonlinear errors. These results indicate that the linear

414 simplification of rotation for the elastomer strain process has a small error for the



415 rotational component but produces a larger wavefield error on the translational
416 components.

417 The linear approximation produces more errors on the translational components
418 obtained from real earthquake simulations, probably because the wavefield energy of
419 rotational component decays faster in natural earthquakes (Lee et al., 2009; Lai and
420 Sun, 2017). Besides, the simulation results of **E2** show a larger difference between
421 linearity and nonlinearity than that of **E1**, which is about ten times larger, mainly
422 because of the increased source energy of **E2**. So, for weak and moderate earthquakes,
423 the effect of nonlinearity may be negligible, and the linear approximation can meet
424 the research accuracy. It can also be attributed to the fact that the two earthquakes
425 have different source mechanisms, which makes its linear approximation error larger.



426
427 **Figure 10.** Relative changes in RMS amplitude of simulation results between linear
428 and nonlinear scenarios for **E1** (a) and **E2** (b)



429

430 **5 Discussions**

431 Compared with the traditional theory of seismic wave propagation in
432 homogeneous elastic media, the Green strain tensor is a function of both the strain
433 tensor and the rotation tensor, as shown in Eq. (5). Without considering the linear
434 approximation of small deformation, the wave propagation equations entail
435 three-order differentiations of displacement, with the higher-order terms influenced by
436 shear modulus and bulk modulus. Given that earthquakes mostly occur in shallow
437 crust or transitional zones between shell and mantle, often considered as planes of
438 elastic attributes transformation and stress discontinuity zones, more intricate media
439 and focal physics (Olson and Apsel, 1982; Olson and Allen, 2005), such as the model
440 featuring a rigid thin-layer sphere (Zhu, 1983), warrant further exploration and
441 discussion.

442 The mechanics of seismic rotation may be related to various factors, including
443 nonlinear elasticity (Guyet and McCall, 1995; Guyet and Johnson, 1999), asymmetric
444 moment tensor (Teisseyre et al., 2003; Teisseyre, 2010), medium heterogeneity,
445 anisotropy (Pham et al., 2010; Sun et al., 2021), and site effects. This study focuses
446 only on isotropic and homogeneous media and three fundamental moment tensor
447 sources in the simulations of nonlinear small deformation. Therefore, the effect of
448 nonlinear geometric relation on wave propagation, especially for rotational
449 components, necessitates further investigation by testing the slipping angle, the shear
450 moment, the elastic parameters, and the anisotropy, among others. The current



451 discussion concentrates on wave propagation and the characteristics of 6-component
452 wavefields excited by three basic moment tensor sources to discuss the theoretical
453 approximation stemming solely from the linear assumption of small deformation, with
454 further analyses of other contributing factors slated for future research endeavors.

455 Observations and simulations of Taiwan Hualien earthquakes have verified the
456 existence of rotational motions along the northeast fault, resulting in prominent
457 Rayleigh-wave recordings and indicative of a vertical slipping mechanism in the
458 earthquake rupture process. In addition, the observation of stronger R_z component and
459 two horizontal components suggests the presence of Love surface waves., signifying
460 clear horizontal slipping and torsion. This finding, aligning with Yu et al.'s (1999)
461 discovery, reveals the existence of horizontal rotational mechanisms within the
462 seismic belt of Taiwan attributed to the Pacific Plate beneath the Eurasian Plate from
463 the east, coupled with northward pressure exerted by the Philippines Sea Plate.

464 The simulations show the nonlinear effect cannot be neglected for near, regional,
465 and strong earthquakes, and that the rotational components observed at ground surface
466 will be stronger than the theoretical one, consistent with previous research.
467 Simulations in this study only portray the sources and medium in a simplified way.
468 The simulations of real earthquake scenarios present a much more intricate interplay
469 of source mechanisms and propagation mediums, encompassing long propagation
470 distances, and long time scales. So, the simulations of observed earthquakes,
471 especially for strong earthquakes, the nonlinear attributes through which seismic
472 waves couple with each other amplify the discrepancies arising from the nonlinear



473 assumption.

474

475 **6 Conclusions**

476 Based on seismic wave equations assuming linear small deformation, we have
477 derived elastic-wave equations that incorporate nonlinear part of Green strain tensor.
478 By numerical simulations in a three-dimensional full-space homogeneous medium
479 model using the finite difference method, our study discusses the distinctive
480 characteristics of translational and rotational motions elicited by three fundamental
481 moment tensor sources, shedding light on the wavefield differences between linear
482 and nonlinear assumptions. The following conclusions can be drawn from our study.

483 (1) Under the influence of the nonlinear Green tensor, the relative displacement,
484 deformation, and strain of spatial mass element in response to external forces are
485 superimposed with nonlinear second-order terms of strain tensor and rotation tensor,
486 resulting in third-order terms of displacement related to the shear and bulk moduli in
487 the propagation of elastic waves.

488 (2) Nonlinearity has a greater effect on ISO and CLVD sources than on DC
489 sources, and the effect of nonlinearity on the wavefield energy increases exponentially
490 with increasing magnitude. The nonlinear effect for ISO source primarily impacts S
491 waves. CLVD source generates wavefield difference ranging from 10 % to 20 % in
492 the 45° diagonal direction of P-wave front, similar to the anomalies caused by media
493 anisotropy.

494 (3) The errors caused by linearity approximation in rotations are more



495 pronounced in pure basic seismic sources. Strong seismic events render the nonlinear
496 effect unbearable in simulations, underscoring the necessity of considering nonlinear
497 effects. In other cases, the linear approximation meets the accuracy requirements, so
498 the linear approximation can be used for relevant questions. Nonlinear small
499 deformation can be a factor in the rotational motion produced by strong earthquakes.

500 (4) The simulation of **E1** and **E2** primarily feature Rayleigh waves in vertical
501 translation and horizontal rotation. However, actual observations indicate a prevalent
502 existence of Love waves, potentially attributable to site effects or more complicated
503 focal mechanisms. The stronger-energy **E2** triggered relatively strong Love waves, so
504 its error caused by the resulting nonlinearity is larger.

505

506 **Author contributions.** WL: conceptualization, methodology, investigation, formal
507 analysis, writing - original draft. YW: conceptualization, writing - original draft and
508 revised draft. CC: in vestigation, formal analysis. LS: methodology.

509

510 **Data and resources.** The seismic records of **E1** are provided by the Institute of Earth
511 Sciences, Academia Sinica, Taiwan, China. The translational records of **E2** are
512 acquired from the Fujian Earthquake Agency.

513

514 **Competing interests.** The contact author has declared that neither of the authors has
515 any competing interes.

516



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519 other geographical representation in this paper.

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521 **Financial support.** This research is financially supported by the National Natural
522 Science Foundation of China (No. 42150201、 No. 62127815、 No. U1839208).

523

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