

An enhanced correlation identification algorithm and its application on spread spectrum induced polarization data

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Abstract. In spread spectrum induced polarization (SSIP) data processing, attenuation of background noise from the observed data is the essential step that improves the signal-to-noise ratio (SNR) of SSIP data. The Time-Domain Spectral Induced Polarization Based on Pseudo-random Sequence (TSIP) algorithm has been proposed to improve the SNR of these data. However, signal processing in background noise is still a challenging problem. We propose an enhanced correlation identification (ECI) algorithm to attenuate the background noise. In this algorithm, the cross-correlation matching method is helpful for the extraction of useful components of the raw SSIP data and suppression of background noise. Then the frequency-domain IP (FDIP) method is used for extracting the frequency response of the observation system. Even when the signal to noise ratio (SNR) is -37.5dB, this ECI algorithm can still be able to keep 3.0% relative error. Experiments on both synthetic and real SSIP data show that the ECI algorithm can not only suppress the background noise but also better preserves the valid information of the raw SSIP data to display the actual location and shape of adjacent high resistivity anomalies, which can improve subsequent steps in SSIP data processing and imaging.

1 Introduction

20 Induced Polarization (IP) technology operated in both the time domain and the frequency domain is useful in exploration for groundwater mapping, mineral exploration, and other environmental studies (Revil 2012, 2019; Høyer et al. 2018). Since the phenomenon of IP in time domain was first discovered by Schlumberger in 1920s, there has been consistent efforts to explore its utilization in various researches. In 1959, the frequency-domain IP (FDIP) approach is proposed by Collett and Seigel, which became the most classic and widely used mapping technique. For example, the first variable-frequency approach was proposed by Wait et al in 1959, then the spectrum approach of the complex resistivity was developed by Zonge and Wynn in 1975, and the dual-frequency IP approach was presented and developed by He et al. in 1993 and Han et al. in 2013. Recently, spread spectrum induced polarization (SSIP) is a popular branch of FDIP which uses pseudo-random current pulses of opposite polarity as an excitation source (Chen et al., 2007; Xi et al., 2013, 2014; He et al. 2015). According to the intrinsic broadband characteristics of the source itself, the spectral response of an observation system can be simultaneously calculated at multiple frequencies in electrical exploration (Liu et al., 2019). Thus, this SSIP technology has been gaining attention and application in electrical prospecting (Xi et al., 2014; Lu et al., 2019; Wang and He, 2020).

SSIP technology has a certain degree of noise immunity, but it is still polluted by inevitable background noise in IP data acquisition. The background noise can be mainly categorized into two types: the Gaussian noise and the impulsive interference with different percentage of outliers (Liu et al., 2016; Kimiaefar et al., 2018; Li et al., 2019). If the background noise is not effectively reduced, the remnant noise can affect the calculation of complex resistivity and may mislead subsequent interpretations of the subsurface structure.

40 The field of FDIP denoising has achieved quite good results through the constant research of experts and scholars. There have been many algorithms that can be used to suppress the FDIP random noise (Mo et al., 2017), such as smooth filter (Guo, 2017), Mean stack (Liu, 2015), digital filter (Meng et al., 2015), and robust stacking (Liu et al., 2016). The smooth can effectively attenuate Gaussian noise, but the impulsive interference with intense energy leaves the effectiveness of this

algorithm limited. Therefore, an effective attenuative algorithm for background noise is still a challenging task for traditional noise suppression algorithms (Neelamani et al., 2008; Liu et al., 2017). SSIP method also faces the same issue (Liu et al., 2016, 2017).

5 Recently, the new algorithm based on a circular cross-correlation method, Time-Domain Spectral Induced Polarization Based on Pseudo-random Sequence (TSIP) algorithm, has also been used to suppress the SSIP noise (Li et al. 2013; Zhang et al. 2020). Due to its effective denoising ability, the identification method has gained more attention and development. However, the TSIP algorithm is restricted because the excitation signal is sensitive to the random noise. For this problem, we propose an enhanced correlation identification (ECI) algorithm for reducing the noise in SSIP data. The ECI algorithm obtains cross-correlations between the transmitter output signal, the excitation signal, and the response signal. The performance of the ECI algorithm is demonstrated on both synthetic and field SSIP data. Experimental results show that the ECI algorithm can effectively control the root mean square of noise (NRMS) increase, enhance its denoising performance in background noise and improve the valid signal preservation to display the actual location and shape of high resistivity anomalies with higher resolution.

2 Theory

15 2.1 Subsection (as Heading 2) The TSIP theoretical model

Figure 1 shows a traditional diagram of the electrical resistivity survey. The transmitter output signal $u_T(t)$ is poured from electrode A to electrode B, the excitation signal $i(t)$ flows from electrode A to electrode B, and the response signal $u(t)$ between the electrodes M and N is measured. To simultaneously obtain the spectral response of subsurface at various frequencies, pseudo-random sequence based the excitation signal $i(t)$ is considered. Thus, the spectral response of subsurface be retrieved by the TSIP algorithm, and its spectral response be expressed as (Li et al., 2013):

$$H_e(\omega) = \frac{P_{ui}(\omega)}{P_{ii}(\omega) \cdot P_s(\omega)}, \quad (1)$$

where $P_{ui}(\omega)$ is the cross-power spectral density of $u(t)$ and $i(t)$, $P_{ii}(\omega)$ the auto-power spectral density of $i(t)$, and $H_s(\omega)$ is the impulse spectral response of the observing system.

25 Given this observation mode using low-power signals, the magnetotelluric system is a time-invariant system and let us suppose that $H_s(\omega)$ is 1. Eq. (1) can further be expressed as:

$$H_e(\omega) = \frac{P_{ui}(\omega)}{P_{ii}(\omega)} = \frac{\text{fft}[R_{ui}(\tau)]}{\text{fft}[R_{ii}(\tau)]} = \frac{U(\omega)}{I(\omega)}, \quad (2)$$

where $\text{fft}[\cdot]$ denotes Fast Fourier Transform (FFT), $R_{ui}(\tau)$ is the cross-correlation function of $u(t)$ and $i(t)$, $R_{ii}(\tau)$ is the auto-correlation function of $i(t)$, $U(\omega)$ and $I(\omega)$ depict the geometric factor defined by the frequency spectrum of $u(t)$ and the frequency spectrum of $i(t)$ respectively, and τ denotes time-delay.

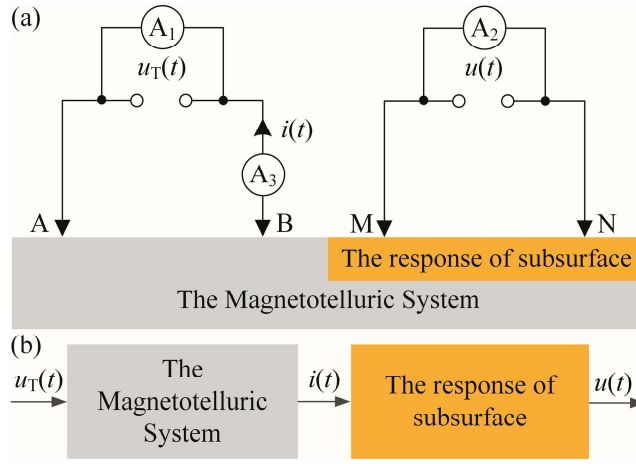


Figure 1. (a) The observation model of the four-electrode measurement. (b) its equivalent diagram.

In the practical field environment, this observation mode is contaminated by the background noise, as shown in Figure2. The output of the sensors A_k ($k=1, 2, 3$) can be expressed as:

$$y_1 = u_T(t) + n_1(t), \quad (3)$$

$$y_2 = u(t) + n_2(t), \quad (4)$$

$$y_3 = i(t) + n_3(t), \quad (5)$$

where $n_k(t)$ is the background noise.

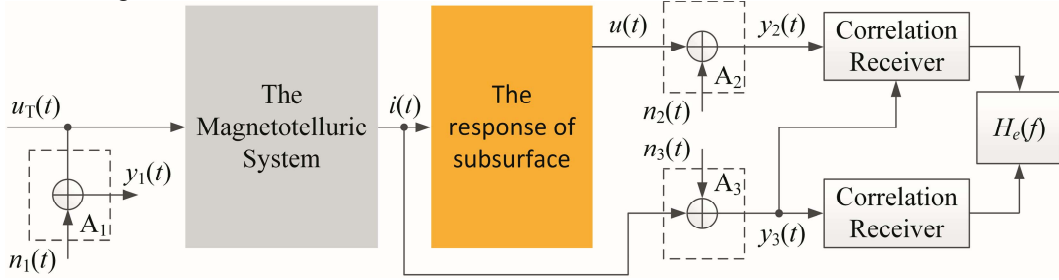


Figure 2. Schematic diagram using the TSIPD algorithm.

Therefore, according to Eq. (2), the formula of the TSIP algorithm is given as:

$$H_e(\omega) = \frac{P_{y_2, y_3}(\omega)}{P_{y_3, y_3}(\omega)} = \frac{\text{fft}[R_{y_2, y_3}(\tau)]}{\text{fft}[R_{y_3, y_3}(\tau)]} = \frac{\text{fft}[R_{ui}(\tau) + R_{un_2}(\tau) + R_{in_1}(\tau)]}{\text{fft}[R_{ii}(\tau) + R_{in_1}(\tau) + R_{n_3, n_3}(\tau)]} \approx \frac{\text{fft}[R_{ui}(\tau)]}{\text{fft}[R_{ii}(\tau) + R_{n_3, n_3}(\tau)]}. \quad (6)$$

Eq. (6) demonstrates that the TSIP algorithm has a weak denoising effect when $n_3(t)$ is the massive intense noise. In other words, the TSIP algorithm depends on the energy intensity of $n_3(t)$ present in $i(t)$.

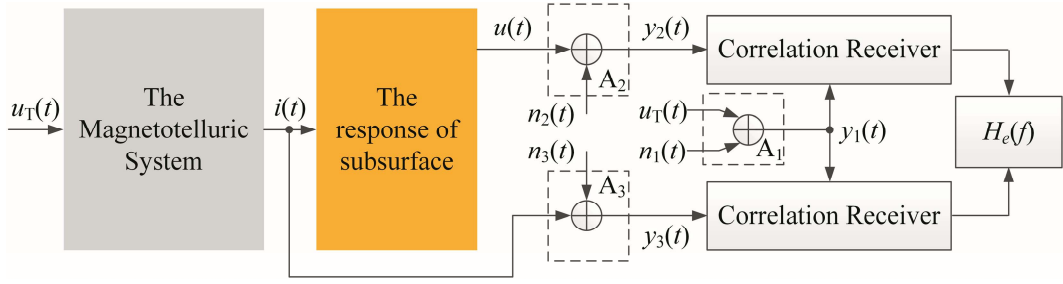


Figure 3. The schematic diagram of the ECI denoising model.

2.2 The ECI theoretical model

That the denoising ability of the TSIP algorithm is limited is caused by that $i(t)$ is sensitive to $n_3(t)$. To solve this problem, the ECI algorithm is proposed and its derivation process is as follows.

Firstly, let us suppose that the telluric system is a time-invariant system under low-power signals. For three sensor output signals, their cross-correlation functions are the periodic correlation functions of time τ . When the length of the correlation window NT is specified, 0.0125s in this experiment. The cross-correlation functions can be expressed as follows:

$$R_{y_1 y_2}(\tau) = E[y_1(t)y_2(t-\tau)] = (R_{u_{T_i}}(\tau))_N + R_{n_1 n_2}(\tau), \quad (7)$$

$$R_{y_1 y_3}(\tau) = E[y_1(t)y_3(t-\tau)] = (R_{u_{T_i}}(\tau))_N + R_{n_1 n_3}(\tau), \quad (8)$$

where $R_{n_1 n_2}(\tau)$ and $R_{n_1 n_3}(\tau)$ are the cross-correlations of $n_2(t)$ and $n_3(t)$ respectively, and τ is time-delay that lies in the range of $-NT$ to NT .

According to the design features of ZW-CMDSII (Zhang, et al., 2014; He, et al., 2014;), $n_1(t)$ caused mainly by the floor noise energy of the instrument is relatively very low, while $n_2(t)$ and $n_3(t)$ possess much higher energy level because they are mainly composed of environment noise. Thus we can assume that the cross-relation between $n_1(t)$ and $n_2(t)$, $n_3(t)$, $R_{n_1 n_2}(\tau) \approx 0$ and $R_{n_1 n_3}(\tau) \approx 0$.

Based on the above analyses, we can further obtain:

$$R_{y_1 y_2}(\tau) \approx (R_{u_{T_i}}(\tau))_N, \quad (9)$$

$$R_{y_1 y_3}(\tau) \approx (R_{u_{T_i}}(\tau))_N. \quad (10)$$

Then the cross-power spectrum of Eq. (9) and Eq. (10) can be written as following

$$P_{y_1 y_2}(\omega) \approx P_{u_{T_i}}(\omega), \quad (11)$$

$$P_{y_1 y_3}(\omega) \approx P_{u_{T_i}}(\omega). \quad (12)$$

Finally, according to Eq. (2) and Eq. (11), Eq. (12) can be expressed as following

$$H_e(\omega) = \frac{U(\omega)}{I(\omega)} = \frac{U(\omega)U_T^*(\omega)}{I(\omega)U_T^*(\omega)} = \frac{P_{u_{T_i}}(\omega)}{P_{u_{T_i}}(\omega)} \approx \frac{P_{y_1 y_2}(\omega)}{P_{y_1 y_3}(\omega)}. \quad (13)$$

So, Eq. (13) is the formula of the ECI algorithm. The derivation process of this formula clearly describes that the ECI algorithm can effectively suppress the background noise and be independent on the degree of $n_3(t)$ present in $i(t)$.

3 Experiment on synthetic SSIP data record

5 We test the ECI algorithm for attenuating background noise of SSIP data sets in comparison with the FDIP algorithm and the TSIP algorithm. For the comparison, the SNR, root mean square of noise (NRMS) and relative error (ε) as the objective parameters to judge the performance of denoising, which are calculated as follows:

$$\text{SNR} = 10 \log_{10} \left\{ \frac{\sum_{i=1}^M [y(i) - \mu_y]^2}{\sum_{i=1}^M [n(i) - \mu_n]^2} \right\}, \quad (14)$$

$$\text{NRMS} = \sqrt{\frac{\sum_{i=1}^M [n(i)]^2}{M}}, \quad (15)$$

$$\varepsilon = 100 \times \frac{\rho_1 - \rho_0}{\rho_0}, \quad (16)$$

$$10 \quad i(t) = u_i(t) / R_s \quad (17)$$

where μ_y and μ_n denote the mean values of the useful signal and the noise separately. $y(i)$ and $n(i)$ are the useful signal and the noise separately, M is the length, ρ_0 denotes the complex resistivity calculated without noise, and ρ_1 is the complex resistivity calculated with the noise added to ρ_0 . R_s is the value of the sampling resistor ($R_s = 1\Omega$), and $u_i(t)$ is the voltage at the sampling resistor.

15 To validate the effectiveness of the ECI algorithm, we test for one practically recorded data set. Firstly, we use the applied voltage $u_T(t)$, the injected current $i(t)$ and the measured potential signal $u(t)$ as the raw signals. These signals are a 3-order spread spectrum pseudo-random sequence at the clock cycle of 0.0125s, as shown in Figures 4a-c. Secondly, In our experiment the measurement line is 19m and in a stable environment, so we consider the system linear time-invariant and the noise from the current and voltage measurement are linearly superpositioned (Pelton, et al., 1983; De, et al., 1983; Vinegar and Waxman, 1984; 20 De, et al., 1992; Garrouch and Sharma, 1998). Therefore, it is actually equivalent whether the noise is added to the injected current $i(t)$, the measured potential signal $u(t)$ or the applied voltage $u_T(t)$. Therefore, the injected current $i(t)$ is only polluted by the synthetic background noise, including Gaussian and impulsive, as shown in Figures 4d and e. Thirdly, the complex resistivity of the main frequency is considered and discussed because the main energy of the pseudo-random signal is concentrated on the main frequency (He, 2017). Finally, for detailed comparisons between the ECI algorithm and the others, we add the synthetic Gaussian and impulsive noises to the response signal $i(t)$, respectively. 25

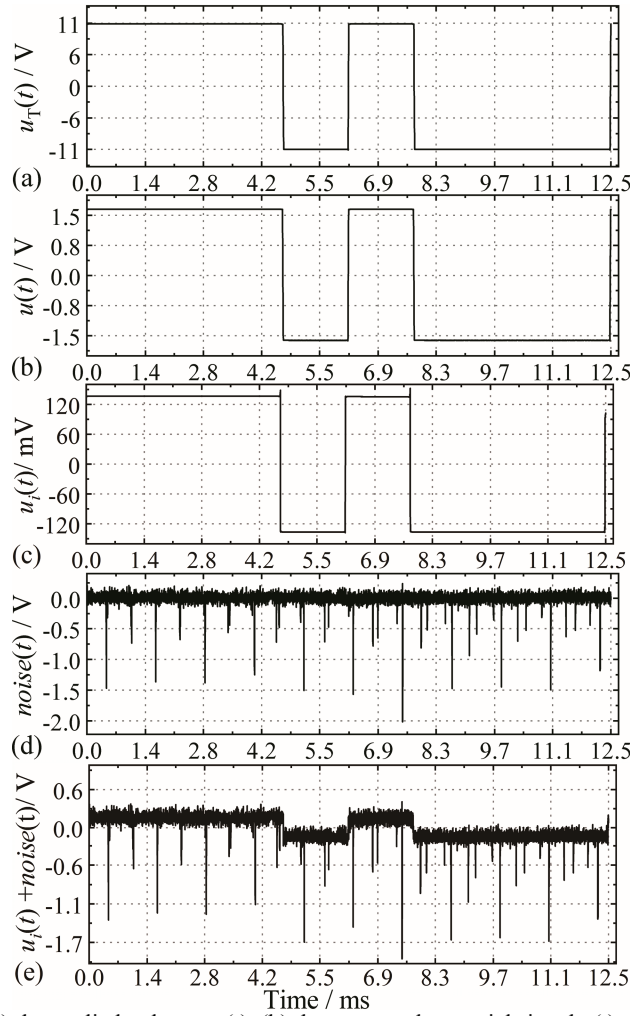


Figure 4. The time waves of (a) the applied voltage $u_T(t)$, (b) the measured potential signal $u(t)$, (c) the voltage $u_i(t)$ at the sampling resistor, (d) noise(t), and (e) the synthetic signal $(u_i(t) + \text{noise}(t))$.

We use synthetic Gaussian noise with the deviation and mean value of 0.1 and 1.1 as a standard template. The excitation signal $i(t)$ is polluted by synthetic different energy levels of the Gaussian noise, as shown in Figure 5. The denoised results obtained by the ECI algorithm and the others are shown in Figures 5a-c. These figures show that the relative error and SNR of the excitation signal $i(t)$ are calculated and compared at the three main frequencies when the noise RMS ranges from 0 to 0.9. From Figure 5b, it can be seen that the denoising ability of TSIP algorithm depends on the energy intensity of the noise presence in the excitation signal $i(t)$, consistent with the conclusion of Eq. (6). Meanwhile, Figure 5 indicates that the ECI algorithm possesses the best denoising performance under the same noise RMS and SNR. Particularly, when the SNR is -37.5 dB, this ECI algorithm is still able to keep 3.0% relative error at the primary frequency 160Hz.

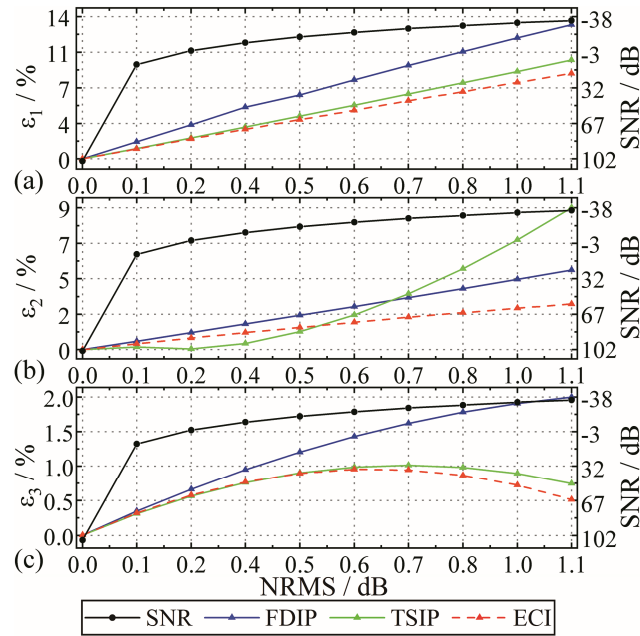


Figure 5. The effect of different degrees of Gaussian noise to the measures excitation signals. (a) SNR of the polluted potential signal. Complex resistivity relative error at (b) 80 Hz, (c) 160 Hz, (d) 320 Hz comparison using the three methods.

Previous literature has shown that if the percentages of outliers in impulsive noise exceed 50%, the traditional denoising algorithm will be limited (Liu et al., 2016, 2017). Thus, Synthetic impulsive noise is added to the excitation signal $i(t)$ in ten percent steps. Their standard deviations (SDs) and skewnesses (SKs) are shown in Figure 6. As depicted in Figures 7, the three algorithms have a certain degree of denoising performance versus the different percentages of the synthetic outliers against the raw data. However, the ECI algorithm still has superior denoising performance and holds smaller fluctuation of the relative error when the percentage of the outliers is more significant than 50%. For example, the average SD in ECI processing the SSIP data is 37% and 51% lower than the FDIP and TSIP respectively.

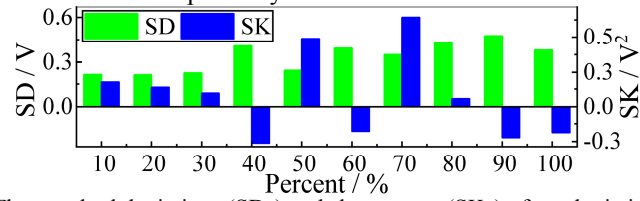


Figure 6. The standard deviations (SDs) and skewnesses (SKs) of synthetic impulsive noise.

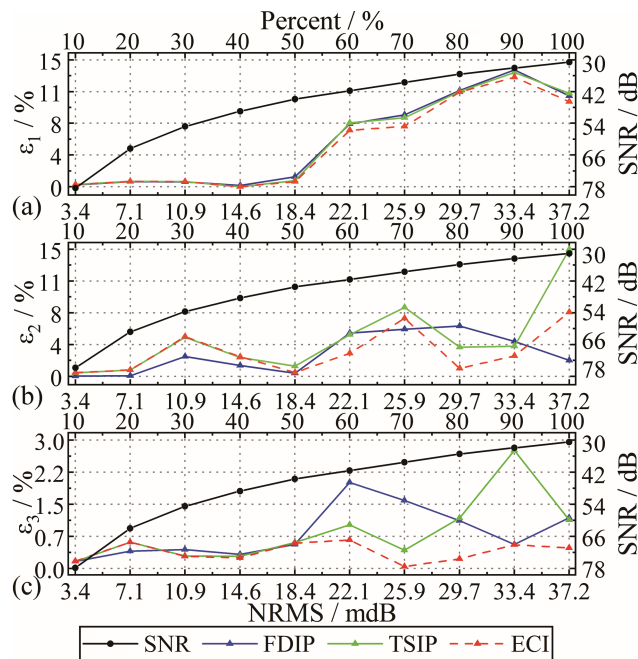


Figure 7. The effect of different levels of spike noises to the measured excitation signals. (a) SNR of the contaminated potential signal in the amplitude-frequency characteristics. Complex resistivity relative error at (b) 80 Hz, (c) 160 Hz, (d) 320 Hz comparison using the three methods.

5 4 Experiment on real SSIP data record

To further verify the performance of the ECI algorithm, the Wenner array, the traditionally applied system in the field, was selected for performing laboratory tests, as shown in Figure 8. SSIP data was acquired with high-density meter and 20 electrodes at 1m spacing. A Wenner acquisition sequence was adopted with 55 potential measurements expressed utilizing the green and points. The figure shows an example of two high resistance cavities. The two cavities were presented by the letters A and B, and their calibers were about 1.8 m × 2 m. The measured excitation signal had a range between 0.04 and 0.19 A approximately. The transmitter output signal is a three-order sequence with 80 Hz frequency, and its voltage is about ± 11.8 V. The sampling frequency is 625 kHz. The excitation and response data of 40 periods were recorded at each point.

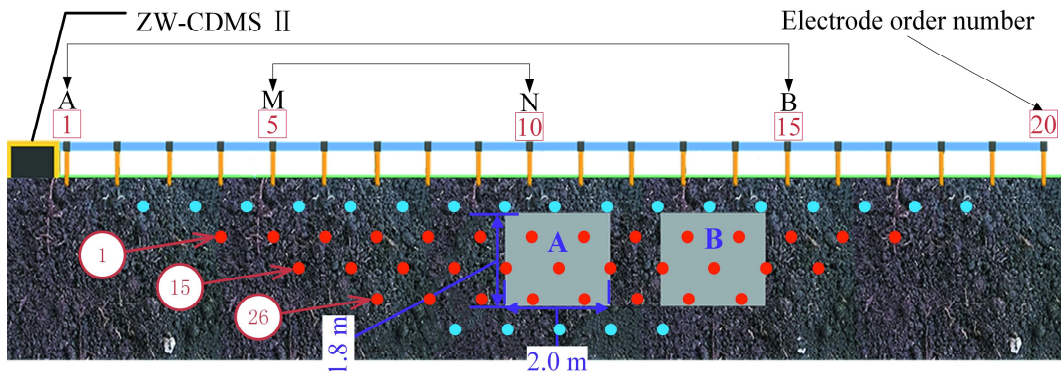
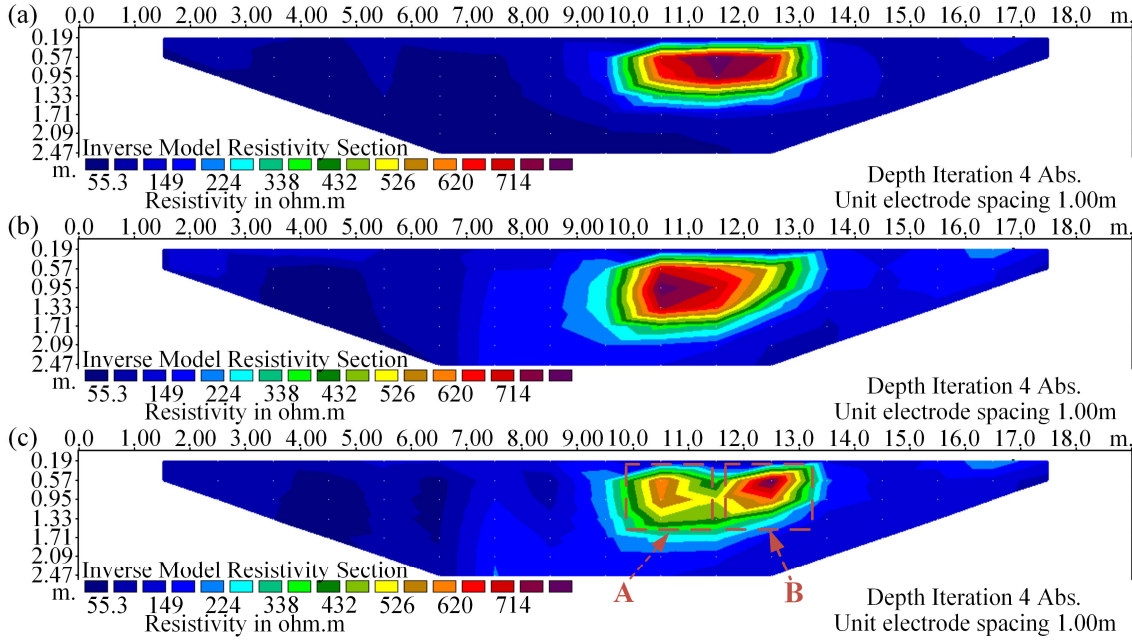


Figure 8. The schematic of the two high resistance cavities.

Figure 9 demonstrates the experimental SSIP data processed by the three algorithms, inverted with Res2DInv. It can be observed that the location and shape of two abnormal bodies are distinguished only in the ECI algorithm while recognized as one whole in the other algorithms. We believe the reason that ECI has higher detection precision is due to its higher denoising ability.

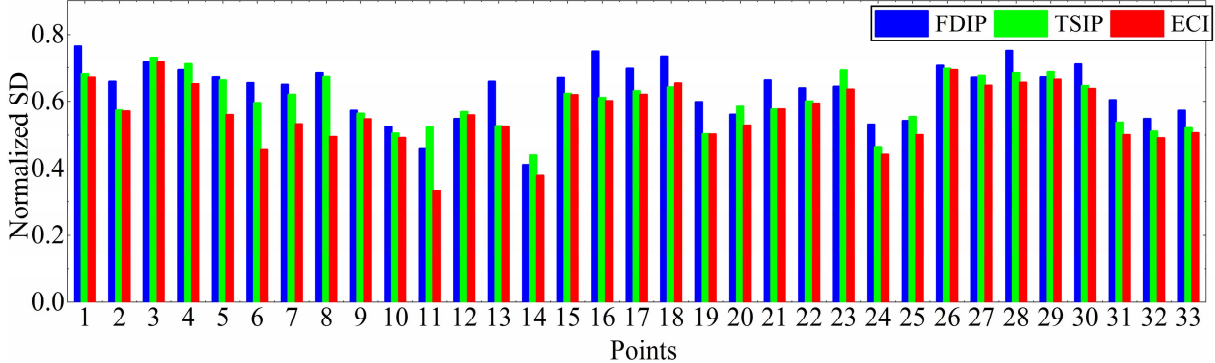


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Figure 9. Inverted resistivity sections of the two high resistivity anomalies (A and B) at 80Hz with using (a) the FDIP method, (b) the TSIP algorithm, and (c) the ECI algorithm.

To verify the reason of the improved detecting precision, the SD for each red point is calculated, as shown in Figure 10. This figure shows that among the 33 SD of SSIP data by processed the ECI method is the lowest at all points except for the 28th. The average SD in ECI processing the SSIP data is 7% and 3.8% lower than the FDIP and TSIP respectively. Also, the maximum value of SDs with the ECI method is 5% and 1.4% lower than the others, and the minimum value is 8% and 10% lower, respectively. These results quantitatively indicate that the ECI algorithm improves the accuracy and robustness of the collected data.

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Figure 10. Standard deviation (SD) of the ECI algorithm and the others to the red data dots at 80Hz.

Meanwhile, amplitude-frequency $|\rho(f)|$ and phase-frequency $\varphi(f)$ characteristics of complex resistivity are calculated by the three algorithm (one period) in survey point No 21, in Figure 11. As depicted in Figure 11, the complex resistivity processed

by the ECI shows a linear trend with the three main frequencies. Also, the SD of the amplitude-frequency $|\rho(f)|$ characteristic is 9.9% and 4.9% lower than the others, and the SD of the phase-frequency $\varphi(f)$ is 356.1% and 3.3% lower. Therefore, we believe that the ECI algorithm has advantage on suppressing background noise, which benefits the subsequent steps in SSIP data processing and imaging.

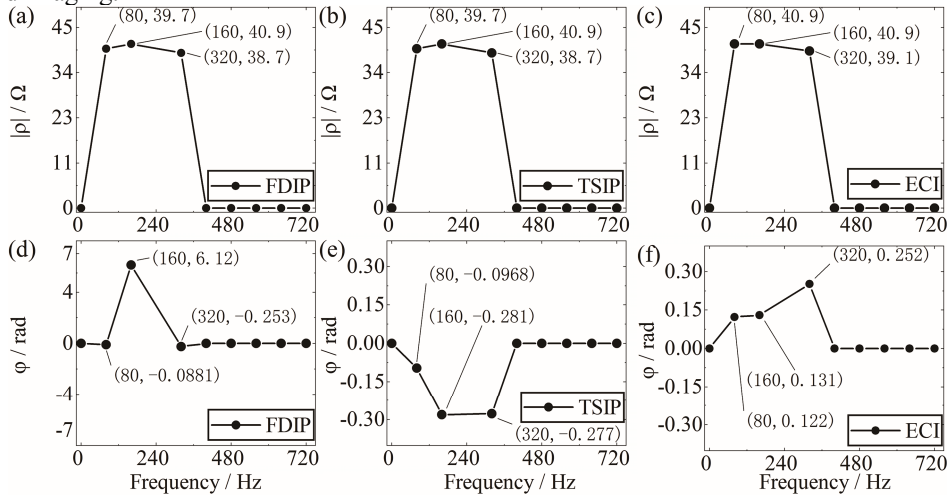


Figure 11. Complex resistivity spectrum calculated by the three algorithm (one period) in survey point No 21.

5 Conclusions

We propose the ECI algorithm that effectively attenuates the background noise in SSIP data and improves the complex resistivity spectrum. This method uses the correlation function to neutralize the influence of the background noise in the SSIP data, and the spectrum complex resistivity can be calculated at multiple frequencies by the formula of the complex resistivity. Simulation results show that the ECI algorithm can effectively attenuate the background noise and improve the SNR. Subsequently, the practicability of the ECI algorithm is further verified by a field test. The results demonstrate that the SD of the SSIP data is improved, which benefits the accuracy and stability of the collected data. There is a good agreement between the complex resistivity and the geological target body with high resistance, which indicates that the ECI algorithm can help to improve the quality of interpretation and inversion in the survey area. The ECI algorithm can more effectively suppress the background noise including the Gaussian random and impulsive noises, but its effect on particular frequency disturbance is very limited due to the periodicity of the disturbance. Therefore, denoising algorithm based on pseudo random sequence correlation identification is still left open for more investigation.

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