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# A Mathematical Framework for the Description of Convection in Meso-scale Synoptic System

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## Abstract

By introducing an appropriately-defined imbalanced vortical flow as the basic state, our previous study has extended conventional instability theories of balanced flows for meso-scale convection. It considered not only the apparent instability of the imbalanced basic state but also the two-way interaction between convection/IGWs and this imbalance. This paper reports our *new progresses* of such framework. A regular perturbation method on the nonlinear case is performed to have an insight into the triggering mechanism of convection. It seems convection can be triggered in resonance either with imbalance forcing or with nonlinear interaction among different modes. Even if all these cannot happen, an imbalance forcing with strong enough magnitude may eventually trigger convection. These are essentially different from the concept of Liyapunov instability, in which an initial disturbance is necessary. In some simplified but relatively general setting, all modes that may contribute to the structures of meso-scale convection are investigated, including free modes of convection and forced modes of convection/IGWs by imbalance. Particularly, the influences of arbitrary distribution of stratification on qualitative properties of free and forced convection/IGW modes are discussed. Also, approximate forms of forced convection/IGW modes suitable for application are given for horizontally uniform stratification. Finally, to demonstrate the potential application of our theory, the concept of imbalance forcing and balanced flow adjustment is shown to be useful in the understanding of key issues in typhoon study, such as its possible role in typhoon's self-organization, Fujiwhara effect and the relationship between typhoon's asymmetric structure and its track recurvature.



## 1 **1 Introduction**

2 Earlier theories attributed the arising of convection to the instabilities of balanced flows such as static  
3 instability, symmetric instability and etc. (Hoskins, 1974; Holton, 1992; Xu and Clark, 1985). However,  
4 many issues of convection still cannot be understood within the perspective of instability because of the  
5 following reasons. First, since classical theory of instability demands basic state must be a strict solution  
6 or exactly balanced flow, previous studies deal with too simple cases of balanced flows (mainly static  
7 state or parallel geostrophic flows with vertical/horizontal shears, see Pedlosky, 1979; Drazin, 1981  
8 Holton, 1992) to have further applications. In real atmosphere, the instability theory for a general basic  
9 state which needs not to be a strict solution or balanced flow is necessary, not only because of the  
10 difficulties in ensuring the existence and finding out the exact solution for a general basic state, but also  
11 because of the highly imbalanced natures in synoptic systems of meso-scales. Second, meso-scale  
12 convection should be considered in the context of its two-way interaction with its basic state of larger  
13 scales (Emanuel et al., 1994; Roode et al., 2004). So, instability with the prescribed basic state as a strict  
14 solution of the nonlinear equations of motion cannot be a suitable description for such interaction as  
15 disturbance can never react on the basic state under this circumstance. Last, in the sense of classical  
16 Liyapunov stability, an extra initial disturbance is necessary for the triggering the instability, while the  
17 existence of such disturbance is hard to be identified in real atmosphere which is an ultimate state of  
18 long time evolution.

19 Our previous work which was motivated by the expectation to tidy these interconnected issues up,  
20 has incorporated meso-scale convective activities in the framework of instability problems of  
21 imbalanced basic state defined appropriately as an imbalanced vortical flow (Zhao, et al, 2011). Both  
22 loss of balance and loss of stability and their influences on the onset, development of convective  
23 activities had been investigated as a preliminary work. However, investigations on many key issues are  
24 still far from sufficient. Some important concepts need to be extended and clarified further and some  
25 key specific issues need to be discussed more sufficiently to enhance the framework. Emphases of this



1 paper are placed on our new progresses in following three issues of convection of imbalanced basic  
2 flows: 1) The triggering mechanism of convection, an key issue of convection that still remains unclear  
3 partly because the mathematical nature of such issue is not well understood in our previous work. By  
4 utilizing a perturbation analysis, an further insight into this issue is conducted and gives interesting new  
5 results; 2) We know that free and forced modes of convection and inertia-gravity waves (hereafter,  
6 referred as IGWs) are essential to understand the structure of convective activities, whereas the  
7 distribution of stratification (stable or unstable) may affect greatly the behaviors of these modes. The  
8 situation of horizontally uniform stratification had been considered in our previous work. However, no  
9 mathematical way is found to cope with the situation of an arbitrarily distributed stratification so as to  
10 draw some general conclusions on these modes. By proposing an linear eigenvalue problem in some  
11 simplified but relatively general setting, we give qualitatively resolution to this issue as well as  
12 interesting conclusions. We believe these linear modes may serve as the basis to understand the  
13 structure of convective activities which is intrinsically nonlinear phenomenon that comprise interaction  
14 among a multitude of such linear modes at various scales and is difficult to be dealt with. In addition,  
15 we also need to modify the results of horizontally uniform stratification that we obtained previously and  
16 transform them into some applicable forms for our subsequent study of application; 3) So far, we don't  
17 have an successful example of application to demonstrate the usefulness of our previous theory, for  
18 which we choose the study of typhoon properties such as its formation and the relationship between  
19 typhoon recurvature and its asymmetric structure as the example.

20 The paper is arranged as follows. In section 2, we give a brief summary of the basic theory and  
21 related concepts of our previous study, and provide the basic equations necessary for our further study  
22 in this paper. In section 3, as an important aspect of two-way interaction of convection with its  
23 environment, triggering mechanism of convection is investigated via a perturbation analysis. We try to  
24 find qualitative properties for convection and IGW modes of some general cases in section 4, where a  
25 arbitrarily distributed stratification with unstable zone included is assumed. In section 5, we consider the



1 special and solvable case of a horizontally uniform stratification with also unstable zone included is  
2 assumed. Rather than only forced convection mode are considered as in Zhao, et al. (2011), all vertical  
3 motions that may contribute to the structure of convection in meso-scale system are given, including  
4 those caused by free modes of instabilities, forced convection and IGWs. The approximate forms that  
5 are applicable for the straightforward estimation of convection/IGW structures inside and outside a  
6 meso-scale system are also derived. In section 6, physical explanations of above results are given so as  
7 to tie them with convective activities of various meso-scale synoptic systems in real atmosphere, which  
8 may service as a brief direction for the potential application of our theory. Particularly, applications in  
9 the explanation of typhoon's structure and motion are provided as an example of detailed study. Section  
10 7 is devoted to a summary and conclusions of the whole paper.

## 11 **2 Basic concepts and related equations of the theory**

12 The basic equations applicable to meso-scale convection system in our previous study (Zhao, et al, 2011)  
13 are vorticity equation, divergence equation and thermodynamic equation in  $p$ -coordinates and  $f$ -plane. For  
14 the simplicity, the forms of these equations and their properties related to balanced flows are given in  
15 Appendix A. Although hydrostatic assumption cannot give the most exact description of each single  
16 small-scale cell of convection, it has the advantages to deal with the structure of meso-scale convective  
17 activity and its interaction with the background. In this sense, this paper actually treat with meso-scale  
18 convective activity. However, above form of basic equations is unable to provide us an intuitive basis for  
19 both the mathematical and physical aspects of the relation between imbalanced basic flow and meso-scale  
20 organized convective activity characterized by convection/IGWs modes. So, by reducing these basic  
21 equations to just one equation, we introduce a new form of equation, in which imbalance, convection/IGWs  
22 and their relation can be recognized more easily. This new equation leads

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$$24 \quad \frac{\partial^2 \delta_{pp}}{\partial t^2} + \sigma \nabla^2 \delta + f^2 \delta_{pp} + \mathfrak{I}(\delta) - \ell_{\zeta, \varphi} \delta = \mathfrak{R}(\zeta, \varphi) \quad (1)$$

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1 Where  $\delta$  is the horizontal divergence,  $\zeta$  the vertical component of vorticity,  $f$  the Coriolis-parameter  
 2 and  $\sigma$  the static stability parameter. The linear and nonlinear operators acting on  $\delta$ , *i.e.*  $\ell_{\zeta, \varphi} \delta$  and  
 3  $\mathfrak{I}(\delta)$  are given as below

$$\begin{aligned} \ell_{\zeta, \varphi} \delta = & [-f \nabla \zeta \cdot \mathbf{V}_\delta - f \frac{\partial \zeta}{\partial p} \omega - f \zeta \delta + f \mathbf{k} \cdot (\frac{\partial \mathbf{V}_\zeta}{\partial p} \times \nabla \omega)]_{pp} \\ & - [\mathbf{V}_\zeta \cdot \nabla \delta + (a_\zeta a_\delta + b_\zeta b_\delta) + \frac{\partial \mathbf{V}_\zeta}{\partial p} \cdot \nabla \omega]_{ppp} + \nabla^2 [\nabla (\frac{\partial \varphi}{\partial p}) \cdot \mathbf{V}_\delta]_p \end{aligned} \quad (2a)$$

$$\begin{aligned} \mathfrak{I}(\delta) = & f [-\mathbf{k} \cdot (\frac{\partial \mathbf{V}_\delta}{\partial p} \times \nabla \omega)]_{pp} - (\mathbf{V}_\delta \cdot \nabla \delta + \omega \frac{\partial \delta}{\partial p} + \frac{\partial \mathbf{V}_\delta}{\partial p} \cdot \nabla \omega)_{ppt} \\ & - \frac{1}{2} (\delta^2 + a_\delta^2 + b_\delta^2)_{ppp} \end{aligned} \quad (2b)$$

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 8 Here,  $\mathbf{V}$  is the horizontal wind with zonal component  $u$  and meridional component  $v$ ,  $\omega$  the vertical wind  
 9 and  $\varphi$  the geo-potential height.  $a = \partial u / \partial x - \partial v / \partial y$  and  $b = \partial v / \partial x + \partial u / \partial y$  are deformations of the  
 10 horizontal wind. The horizontal wind speed can be decomposed into vortical and divergent parts, *i.e.*,  
 11  $\mathbf{V} = \mathbf{V}_\zeta + \mathbf{V}_\delta$ , where the mean or constant part of the wind speed is absorbed into  $\mathbf{V}_\zeta$ . The subscript  $t$  and  $p$   
 12 denote the partial derivative with respect to them. On the right-hand side of (1),

$$\mathfrak{R}(\zeta, \varphi) = -\frac{1}{2} [(a_\zeta^2 + b_\zeta^2 - \zeta^2)_t]_{ppp} - f (\mathbf{V}_\zeta \cdot \nabla \zeta)_{pp} + \nabla^2 [\mathbf{V}_\zeta \cdot \nabla (\frac{\partial \varphi}{\partial p})]_p \quad (3)$$

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 16 is the inhomogeneous term which depends only on  $(\zeta, \varphi)$ . Since vorticity equation, divergence equation  
 17 and thermodynamic equation are substituted into (1) in the derivation, constraints from basic dynamical  
 18 and thermo-dynamical laws that one might expect in convective systems in the real atmosphere still work  
 19 to a certain extent in (1). Nevertheless, equation (1) is more appropriately to be regarded as a diagnostic  
 20 equation for the qualitative relationship between imbalanced basic flow and convection/IGWs. Although it



1 alone is not closed and cannot serve as the governing equation to determine the motion, it does serve as one  
2 of the constraints for the motion. In another words, it may unable to describes all aspects of the motion, but  
3 it can describes qualitatively one aspect: the relationship between unbalanced basic flow and  
4 convection/IGWs.

5 The balanced flow is a purely vortical flow with  $\delta=0$  and is delineated just by  $(\zeta, \varphi)$ . Obviously,  
6 staticstate, parallel geostrophic flow and axisymmetric gradient flow are just particular cases of balanced  
7 flows. One of the key points of our previous work is that we decompose the phase state  $S$  of the dynamical  
8 system as below

$$10 \quad \mathbf{S} \equiv \begin{pmatrix} \delta \\ \zeta \\ \varphi \end{pmatrix} = \begin{pmatrix} 0 \\ \zeta \\ \varphi \end{pmatrix} + \begin{pmatrix} \delta \\ 0 \\ 0 \end{pmatrix} \equiv \mathbf{S}_0 + \mathbf{S}' \quad (4)$$

11

12 where  $S_0$  is the basic state and  $S'$  the disturbance. In other words,  $(\zeta, \varphi)$ , the vortical component  $\zeta$  together  
13 with  $\varphi$  is viewed as a generalized basic state, regardless whether or not they are exactly balanced, while  
14 the divergent component  $\delta$  is the disturbances about it.

15 It is proven that, if the basic state  $(\zeta, \varphi)$  is an exactly balanced flow or an exact solution, we have  
16  $\Re(\zeta, \varphi) = 0$ , then (1) returns to the original problem of instabilities including static instability and  
17 symmetric instability *etc.* The corresponding types of linear instabilities with  $\Im(\delta)$  omitted are given in  
18 Table I. However, the exactly balanced flows are just particular cases. In a meso-scale system, the basic  
19 state  $(\zeta, \varphi)$  may remains far apart from balance or even no such solution of balanced flow can exist.  
20 Under such circumstances the inhomogeneous term remains  $\Re(\zeta, \varphi) \neq 0$  in (1), which appears as some  
21 external forcing of the basic state on convection. As a result, in addition to producing instabilities, the role  
22 of imbalanced basic flow on convection seems also to be a forcing by its imbalance. These are even more  
23 clearly seen from the quasi-linear version of (1) without  $\Im(\delta)$ , namely



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$$\frac{\partial^2 \delta_{pp}}{\partial t^2} + \sigma \nabla^2 \delta + f^2 \delta_{pp} - \ell_{\zeta, \varphi} \delta = \mathfrak{R}(\zeta, \varphi) \quad (5)$$

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Its solution is the superposition of homogeneous solution  $\delta_h$  and inhomogeneous solution  $\delta_i$ , *i.e.*

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$$\delta = \delta_h + \delta_i \quad (6)$$

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The homogeneous part of (5) and its solution  $\delta_h$  behave like a problem of linear instability of the basic state  $(\zeta, \varphi)$ , even if  $(\zeta, \varphi)$  is not an exactly balanced flow having  $\mathfrak{R}(\zeta, \varphi) \neq 0$ , which is called by us an *apparent* instability because the original concept of stability/instability is for balanced flow or exact solution. Meso-scale convection is related with this kind of apparent instability having nearly the form of static instability, Kelvin-Helmholtz instability, inertia instability or symmetric instability *etc.* The inhomogeneous solution  $\delta_i$  of (5) for an unstable homogeneous operator is different from that of a stable one of forced IGWs or spontaneous emission (Lighthill 1952; Ford, 2002). So both the homogeneous and the inhomogeneous solution contribute to the meso-scale convection. Consequently, rather than the traditional way which defines convection as the vertical motion arising from the instabilities of exactly balanced flows, the generalized definition regards convection as the results of both apparent instability and the response to the forcing of an imbalanced basic flows with such apparent instability. On the whole, by using a quasi-linear version of the basic equation, we can decouple instability and response to imbalance. As a result, smaller scale of instability and larger scale imbalance of  $(\zeta, \varphi)$  are separated as well. As  $(\zeta, \varphi)$  and its imbalanced is mainly at meso-scale, it can serve as a basic flow of the convective activities.

### 3 Triggering of convection and its interaction with basic flow

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The characters concerning interaction between convection and its basic imbalanced vortical flow depend highly on development stages of convection (Tao *et al*, 1979). Characters of such interaction for *developed*





1 stage of convection are not the whole story. The *triggering* mechanism of the convection is another aspect  
2 that constitutes the issue of two-way interaction. Both of these two aspects will be discussed in this section.

### 3 *3.1 Two-way interaction: developed convection*

4 Equation (1) actually describes implicitly a two-way interaction between convective activities and the  
5 basic flow as well. Generally speaking, the reaction or feedback of the convection on the basic flow seems  
6 far more complex to be described in the full nonlinear form of  $\delta$ . For the simplicity, we just consider the  
7 quasi-linear case of this issue given by (5). But this does not need to mean the discussion is in linear sense,  
8 because  $\ell_{\zeta, \varphi} \delta$  and  $\mathfrak{R}(\zeta, \varphi)$  are nonlinear terms. Under this circumstance, it is clear that 1) the free  
9 convection given by homogeneous solution cannot react on the basic flow, and 2) convective activities do  
10 act on the basic flow via forced convection and contribute to its adjustment, which is described by the  
11 reconciliation between the left and right hand sides of (5), although such two-ways interaction can never be  
12 dealt with in the framework of dynamical instabilities. In the present study we would like to address this  
13 issue mathematically as below.

14 According to the Fredholm alternative (see any text book on partial differential equation, e.g. Haberman,  
15 2003), the solvability of (5) requires its inhomogeneous term  $\mathfrak{R}(\zeta, \varphi)$  to be orthogonal to the homogeneous  
16 solution  $\delta_h$ , namely

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$$\langle \delta_h, \mathfrak{R}(\zeta, \varphi) \rangle = \int_{\Omega} \delta_h^* \mathfrak{R}(\zeta, \varphi) d\Omega = 0 \quad (7)$$

19 where  $\langle \cdot, \cdot \rangle$  is an inner product properly defined over some spatiotemporal domain  $\Omega$ , This constraint on  
20  $\mathfrak{R}(\zeta, \varphi)$  means that the imbalance is limited to some certain ways. We suppose the physical meaning of this  
21 reaction of forced  $\delta$  on  $(\zeta, \varphi)$  is related to balanced flow adjustment, which tends to remove the imbalance  
22 of  $(\zeta, \varphi)$  and is the foundation of our application study in this paper.

23 The (approximate) satisfaction of solvability condition (7) also implies equation (1) can be approximated  
24 by its quasi-linear form (5). So when (7) is even not satisfied approximately, it means that: 1) a resonance



1 between convection and imbalance basic flow happens and can be explained as another kind of manner of  
2 this interaction; 2) equation (1) can no longer be approximated by (5) and a fully nonlinear form of  $\delta$  is  
3 needed, which may corresponding to strong convection.

4  
5 *3.2 Triggering mechanism of meso-scale convection*

6 The triggering mechanisms of convection for balanced and imbalanced basic state are different. In the  
7 balanced case, convection or instability grows from some initial disturbance about the state and is called as  
8 a disturbance-triggered convection. In the imbalanced case, convection is a result of both apparent  
9 instability and response to imbalanced forcing. In the linear regime of the development of convection, this  
10 imbalance-forced part of convection ( $\delta_i$ ) cannot interact with free unstable modes of apparent instability  
11 ( $\delta_h$ ). If there is not an initial disturbance for  $\delta_h$ ,  $\delta_h = 0$  is always a solution of the homogeneous equation  
12 and instability can never arise. So an initial disturbance for  $\delta_h$  is also necessary for the development of  
13 apparent instability, which is similar to the case of balanced vortical flows and can also be called a  
14 disturbance-triggered convection. In addition to the old question of where this initial disturbance comes  
15 from, another question leads us to doubt the disturbance-triggered mechanism of convection in real  
16 atmosphere is that: instability should develops immediately once the atmosphere become unstable, while it  
17 seems instability does not raise until some forcing of uplift strong enough happens in observation.  
18 Therefore, theory of disturbance-triggered instability for balanced flow or linear regime of imbalanced flow  
19 need to be improved to explain the triggering of convection. For this purpose, a nonlinear theory for  
20 imbalanced flow is necessary as below.

21 Suppose imbalance around a balanced flow  $(\zeta_0, \varphi_0)$  is weak in equation (1), we then have

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$$\Re(\zeta, \varphi) \propto \varepsilon \quad (8)$$



1 where  $\varepsilon \ll 1$  is a small dimensionless number. Notice also that

2 
$$\ell_{\zeta, \varphi} = \ell_{\zeta_0, \varphi_0} + \ell^1_{\zeta, \varphi} \quad (9)$$

3 *i.e.* operator  $\ell_{\zeta, \varphi}$  can be divided into a balanced and an imbalanced parts. It can also be shown

4 
$$\ell^1_{\zeta, \varphi} \propto \varepsilon \quad (10)$$

5 The perturbation solution of equation (1) is written as

6 
$$\delta = \delta_0 + \delta_1 \varepsilon + \delta_2 \varepsilon^2 + \dots \quad (11)$$

7 Substituting it into (1), we have

8  $\varepsilon^0:$

9 
$$L(\delta_0) - \mathfrak{I}(\delta_0) = 0 \quad (12)$$

10  $\varepsilon^1:$

11 
$$L(\delta_1) = \mathfrak{R}(\zeta, \varphi) + \ell^1_{\zeta, \varphi} \delta_0 + \mathfrak{I}_1(\delta_0) \quad (13)$$

12  $\varepsilon^2:$

13 
$$L(\delta_2) = \ell^1_{\zeta, \varphi} \delta_1 + \mathfrak{I}_2(\delta_0, \delta_1) \quad (14)$$

14  $\dots\dots$

15  $\varepsilon^n:$

16 
$$L(\delta_n) = \ell^1_{\zeta, \varphi} \delta_{n-1} + \mathfrak{I}_n(\delta_0, \delta_1, \dots, \delta_{n-1}) \quad (15)$$

17 where we denote

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1 
$$L(\cdot) = \frac{\partial^2(\cdot)_{pp}}{\partial t^2} + \sigma \nabla^2(\cdot) + f^2(\cdot)_{pp} - \ell_{\varepsilon_0, \varphi_0}(\cdot)$$
 (16)

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Solution of equation at order  $\varepsilon^n$  is a superposition of homogeneous and inhomogeneous solutions, *i.e.*

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5 
$$\delta_n = \delta_{nh} + \delta_{ni}$$
 (17)

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7 And it is easy to show  $\delta_0 = 0$  is a solution of the first equation. So, we have

8 
$$\begin{aligned} \delta &= \delta_1 \varepsilon + \delta_2 \varepsilon^2 + \dots \\ &= (\delta_{1h} + \delta_{1i}) \varepsilon + (\delta_{2h} + \delta_{2i}) \varepsilon^2 + \dots \\ &= \delta_{ist} + \delta_{frc} \end{aligned}$$
 (18)

9 where

10

11 
$$\delta_{ist} = \delta_{1h} \varepsilon + \delta_{2h} \varepsilon^2 + \dots$$
 (19a)

12 
$$\delta_{frc} = \delta_{1i} \varepsilon + \delta_{2i} \varepsilon^2 + \dots$$
 (19b)

13 are defined according to their governing equations as the instability and response to imbalance,  
 14 respectively. This superposition relation is similar to that of linear case in (6). If at some initial time we  
 15 have  $\delta_{ist}|_{t=0} \neq 0$ , instability can be triggered, which is the situation of disturbance-triggered mechanism.

16 Otherwise, if at some initial time  $t = 0$  we have

17

18 
$$\delta_{ist}|_{t=0} = \delta_{1h}|_{t=0} = \delta_{2h}|_{t=0} = \dots = 0$$
 (20)

19

20 then  $\delta_{ist} \equiv 0$ . In the latter case, once forced solution

21



1 
$$\delta_{frc} = \delta_{1i}\varepsilon + \delta_{2i}\varepsilon^2 + \dots \quad (21)$$

2

3 converges and exists, instability cannot be triggered. Conditions for solvability, according to the  
 4 Fredholm alternative, should be

5

6 i) 
$$\int_{\Omega} \Delta^* \Re(\zeta, \varphi) d\Omega = 0 \quad (22a)$$

7 ii) 
$$\int_{\Omega} \Delta^* [\ell_{\zeta, \varphi}^1 \delta_{n-1} + \mathfrak{F}_i(0, \delta_1, \dots, \delta_{n-1})] d\Omega = 0 \quad (22b)$$

8

9 iii) 
$$\delta_{1i}\varepsilon + \delta_{2i}\varepsilon^2 + \dots \text{ converges} \quad (22c)$$

10

11 where  $\Delta$  is the homogeneous solution of  $L(\Delta) = 0$ , while  $\Delta^*$  is its adjoint solution. On the contrary,  
 12 when one of above conditions is not satisfied, instability arises. In fact, once solution  $\delta_{frc}$  does not exist,  
 13 it implies solution  $\delta_{ist} = 0$  can exist neither. So we begin to have  $\delta_{ist} \neq 0$  and instability can thus arises  
 14 under unstable situation. Here, unsatisfication of i) and ii) may be explained as convection's resonance  
 15 for forcing from imbalance and nonlinear interaction among IGW modes, respectively. The phrase  
 16 "resonance" here seems too intangible to be related to the real problem. So we explain it in another ways  
 17 as below. Condition i) and ii) are explained as orthogonal relations between free mode of convection  
 18 and imbalance forcing or forcing by nonlinear interaction of IGW modes, they can further be explained  
 19 as no resemblance, or no correlation between the two space-time fields in the sense of statistics. As a  
 20 result, "resonance" or unsatisfication of i) and ii) can be explained as caused by some resemblance, or  
 21 statistical correlation between the space-time structures of free mode of convection and forcing either  
 22 from imbalance or from nonlinear interaction among IGW modes. Even if no such resonances can  
 23 happen, point iii) suggests the magnitude of imbalance (characterized by  $\varepsilon$ ) be influential. As  $\varepsilon$ -order



1 imbalance becomes strong enough, there may be a critical value  $\varepsilon_c$ . When  $\varepsilon < \varepsilon_c$ , solution  $\delta_{fc}$  exists  
2 together with  $\delta_{ist} = 0$  and convection cannot arise. While once  $\varepsilon > \varepsilon_c$ , solution  $\delta_{fc}$  can no longer exist  
3 and also  $\delta_{ist} \neq 0$ , convection then arises. This explains well the time delay of the development of  
4 convection after the atmosphere becomes unstable. The particular case of triggering mechanism of  
5 convection for balanced flow without meso-scale synoptic systems accompanied, such as daytime  
6 heating on a flat and homogeneous surface, can also be interpreted by these results. In this case we have  
7 both  $\Re(\zeta, \varphi) = 0$  and  $\ell_{\zeta, \varphi} = 0$ , so condition i) is satisfied automatically. If there are IGWs traveling  
8 through the region considered from outside and condition ii) is not satisfied, the nonlinear interaction  
9 among IGW modes may trigger unstable convection modes. A simple analysis as below is helpful for  
10 the imaging of this situation. If  $\sigma$  is  $p$ -dependent, suppose the linear IGW mode is  $P_l(p)e^{-i\omega t}e^{ikx}$ , it  
11 produces a forcing with a portion of  $P_l^2(p)e^{-i2\omega t}e^{i2kx}$  due to quadric nonlinearity. It is easy to show  
12 this portion of forcing cannot be orthogonal to the unstable linear normal mode of convection  
13  $P_c(p)e^{i\omega t}e^{i2kx}$ , as long as vertical  $P_c(p)$  is not orthogonal to  $P_l^2(p)$ , which is usually true because  
14 vertical mode  $P_c(p)$  is already orthogonal to  $P_l(p)$  and can no longer be orthogonal to its  
15 square. This case makes the physical meaning of point ii) even clear, regardless of IGWs is from outside  
16 or generated by meso-scale imbalance itself. This is also consistent with our knowledge before. It has  
17 been long for people to know IGWs is a triggering mechanism for convection in atmosphere with  
18 conditional unstable stratification (see, e.g. Li, 1978). Although there are different explanations for this  
19 fact, resonance between convection and nonlinear interaction among IGWs may be another possible. On  
20 the other hand, unsatisfication of either i) or iii) indicates the role of imbalance forcing in triggering  
21 convection via its structure or magnitude, respectively. This is also well-known fact by forecasters and  
22 referred to imbalance forcing crudely as an uplifting effect by meso-scale circulation, without  
23 distinguishing between the two cases.

24 For this triggering mechanism of the apparent instability, an external initial disturbance is not



1 necessary, because we always have an initial disturbance  $\delta_{ist} |_{t=0} \neq 0$  due to the nonexistence of forced  
 2 solution  $\delta_{frc}$  for the imbalanced vortical flow. Then, imbalance can provide also an initial disturbance  
 3 from which the apparent instability or convection can develop. So, the triggering mechanism of  
 4 convection is attributed to the imbalance of the basic state rather than to some initial disturbance from  
 5 outside. We call this kind of convection without external initial disturbance a spontaneous convection.  
 6 A most important difference between the properties of disturbance-triggered and spontaneous  
 7 convection is that the former develops immediately no matter how small and what kind of structure the  
 8 initial disturbance may be, while the triggering and development of the latter depends highly on the  
 9 structure and strength of the imbalance and nonlinearity.

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#### 4 Some general properties of simplified meso-scale convection system

12 As we have known in above, the relationship between convection and its meso-scale basic flow is  
 13 characterized both by a response to imbalanced forcing  $\mathfrak{R}(\zeta, \varphi)$  and by the apparent instability of the  
 14 basic flow associated with  $\ell_{\zeta, \varphi} \delta$ . When imbalance departure from a balanced flow  $(\zeta_0, \varphi_0)$  is weak,  
 15 the above discussion (equation (13) with  $\delta_0 = 0$ ) suggests the first order linear approximation of (1) can  
 16 be written as

17

$$18 \quad \frac{\partial^2 \delta_{pp}}{\partial t^2} + \sigma \nabla^2 \delta + f^2 \delta_{pp} - \ell_{\zeta_0, \varphi_0} \delta = \mathfrak{R}(\zeta, \varphi) \quad (23)$$

19

20 There are two typical cases of the balanced flow  $(\zeta_0, \varphi_0)$  in meso-scale system. The first one is  
 21 symmetric balanced flow along a variable  $\alpha$ , *i.e.*  $\partial \zeta_0 / \partial \alpha = \partial \varphi_0 / \partial \alpha = 0$ . Here  $\alpha = x \in (-\infty, \infty)$  or  $\alpha = \theta \in$   
 22  $[0, 2\pi)$  correspond to balanced parallel geostrophic wind or concentric gradient wind. Suppose  
 23 disturbance  $\delta$  in above is arbitrary. An average with respect to  $\alpha$  over its whole domain can change (23)  
 24 into a problem of forced symmetric instability, namely



25

$$\frac{\partial^2 \bar{\delta}_{pp}}{\partial t^2} + A\bar{\delta}_{\beta\beta} + B\bar{\delta}_{\beta p} + C\bar{\delta}_{pp} + E\bar{\delta}_{\beta} + F\bar{\delta}_p = \bar{\mathfrak{R}}(\zeta, \varphi) \quad (24)$$

27

28

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32

where  $\beta = y$  or  $\beta = r$  for balanced parallel geostrophic wind and concentric gradient wind, respectively. And coefficient from  $A$  through  $F$  depend on  $(\zeta_0, \varphi_0)$ . Then we have symmetric instability as the homogeneous solution and inhomogeneous forced convection. Conditions for the symmetric instability are

33

$$q = 4AC - B^2 < 0 \text{ when } A > 0 \quad (25)$$

34

35

36

37

Since the steady form of the governing equation (24) under such conditions becomes hyperbolic, the forced convection can no longer be estimated from the structure of forcing  $\bar{\mathfrak{R}}(\zeta, \varphi)$ , unlike the elliptic equation when the equation is symmetrically stable.

38

39

40

The second case is in the highly imbalanced situation that one cannot find a symmetric balanced flow  $(\zeta_0, \varphi_0)$  close to  $(\zeta, \varphi)$  like above. Under this circumstance, it is convenient to choose static basic state  $(\zeta_0 = 0, \varphi_0 = \text{const.})$  horizontally as the nearest balanced flow and have  $\ell_{\zeta_0, \varphi_0} = 0$ , which yields

41

$$\frac{\partial^2 \delta_{pp}}{\partial t^2} + \sigma \nabla^2 \delta + f^2 \delta_{pp} = \mathfrak{R}(\zeta, \varphi) \quad (26)$$

43

44

45

46

47

Its homogeneous part is equal to an issue of static instability (IGWs) when  $\sigma < 0$  ( $\sigma > 0$ ) in some domain of atmosphere. This is a very useful setting in the application study in this paper. So in such a setting, properties of convection/IGWs depend highly on the distribution of  $\sigma$ . If  $\sigma$  is  $p$ -dependent only, its forced solution becomes solvable in spite of its steady part being a hyperbolic equation, which was





1 discussed previously in Zhao et al (2011) and will be improved in detail in the next section. But if there  
2 are regionally confined unstable stratification in meso-scale system, it seems difficult to solve (26). To  
3 address this issue, this section will be focused on the relatively general case of  $\sigma$  being both  $p$ - and  
4 horizontal-dependent arbitrarily and just give some qualitative properties of convection and IGW  
5 modes.

6

#### 7 *4.1 Linear modes of convection/IGW of arbitrarily distributed stratification*

8 We assume both  $p$ - and horizontal-dependent  $\sigma(x, y, p)$  in equation (26) in our following  
9 discussion. First of all, homogeneous part of equation is essential because 1) it decides the free modes  
10 of convection/IGW and 2) such modes together with the structure of inhomogeneous forcing jointly  
11 decide the existence of the forced convection via conditions for solvability (22a) and decide the actual  
12 structure of the forced convection via inhomogeneous solution if it exists. So the homogeneous solution  
13 of (26) is the foundation for the present issues and can be obtained by method of separation of variables  
14 written as  $\delta_n = T_n(t)A_n(x, y, p)$ , so we have

15

$$16 \quad \frac{T_{ntt}}{T_n} + f^2 = -\frac{\sigma \nabla^2 A_n}{A_{npp}} = -\lambda_n \quad (27)$$

17

18 which yields an eigenvalue problem as below

19

$$20 \quad \sigma \nabla^2 A_n - \lambda_n \frac{\partial^2 A_n}{\partial p^2} = 0 \quad (28)$$

21

22 while the temporal part  $T_n$  satisfies

23



$$1 \quad \frac{d^2 T_n}{dt^2} + (\lambda_n + f^2) T_n = 0 \quad (29)$$

2

3 In the appendix B of this paper, it is proven that the real and imaginary parts of  $\lambda_n$  are

4

$$5 \quad \text{Re}(\lambda_n) = \frac{\lambda_n + \lambda_n^*}{2} = \frac{\int_{\Omega} (\sigma \|\nabla A_n\|^2 - 1/2 \|A_n\|^2 \Delta \sigma) d\Omega}{\int_{\Omega} \|\partial A_n / \partial p\|^2 d\Omega} \quad (30a)$$

$$6 \quad \text{Im}(\lambda_n) = \frac{\lambda_n - \lambda_n^*}{2} = \frac{\int_{\Omega} \nabla \sigma \cdot (A_n^* \nabla A_n - A_n \nabla A_n^*) d\Omega}{2 \int_{\Omega} \|\partial A_n / \partial p\|^2 d\Omega} \quad (30b)$$

7

8 respectively. Here,

9

$$10 \quad \int_{\Omega} (\cdot) d\Omega = \iint_S \int_0^{p_s} (\cdot) dp dS; \quad \Omega = S \times [0, p_s] \quad (31)$$

11

12  $S$  is the area of meso-scale system, while  $p_s$  the surface pressure. By introducing an approximate

13 relation of  $\sigma$

14

$$15 \quad \Delta \sigma \approx -const.^2 \sigma \quad (32)$$

16

17 (30a) becomes

18

$$19 \quad \text{Re}(\lambda_n) \approx \frac{\int_{\Omega} (\|\nabla A_n\|^2 + 1/2 const.^2 \|A_n\|^2) \sigma d\Omega}{\int_{\Omega} \|\partial A_n / \partial p\|^2 d\Omega} = \frac{I_n^{positive} - I_n^{negative}}{\int_{\Omega} \|\partial A_n / \partial p\|^2 d\Omega} \quad (33)$$



1

2 Here,

3

$$I_n^{positive} = \int_{\Omega_{\sigma \geq 0}} (\|\nabla A_n\|^2 + 1/2 \text{const.}^2 \|A_n\|^2) \sigma d\Omega \quad (34a)$$

4

$$I_n^{negative} = \int_{\Omega_{\sigma < 0}} (\|\nabla A_n\|^2 + 1/2 \text{const.}^2 \|A_n\|^2) |\sigma| d\Omega \quad (34b)$$

5

6 are integrations over two sub-domains with  $\sigma \geq 0$  and  $\sigma < 0$ , respectively. As a result, if  $I_n^{positive} \geq I_n^{negative}$ ,

7 then  $\text{Re}(\lambda_n) \geq 0$ . Otherwise if  $I_n^{positive} < I_n^{negative}$  we have  $\text{Re}(\lambda_n) < 0$ . A particular case in which

8 approximate relation (32) becomes unnecessary is that  $\sigma = \sigma(p)$  and  $\nabla \sigma = \Delta \sigma = 0$ , namely  $\sigma$  is

9 horizontally uniform. From (30) we have

10

$$\text{Re}(\lambda_n) = \frac{\int_{\Omega} \sigma \|\nabla A_n\|^2 d\Omega}{\int_{\Omega} \|\partial A_n / \partial p\|^2 d\Omega} = \frac{I_n^{positive} - I_n^{negative}}{\int_{\Omega} \|\partial A_n / \partial p\|^2 d\Omega} \quad (35a)$$

11

$$\text{Im}(\lambda_n) = 0 \quad (35b)$$

12

13

14 Then  $\lambda_n$  is real, and in such situation

15

$$I_n^{positive} = \int_{\Omega_{\sigma \geq 0}} \sigma \|\nabla A_n\|^2 d\Omega \quad (36a)$$

16

$$I_n^{negative} = \int_{\Omega_{\sigma < 0}} |\sigma| \|\nabla A_n\|^2 d\Omega \quad (36b)$$

17

18 If  $\sigma > 0$  everywhere, we have always  $\text{Re}(\lambda_n) > 0$ . But if  $\sigma < 0$  in some domain of the atmosphere, one can

19 always find both modes with  $\text{Re}(\lambda_n) > 0$  and modes with  $\text{Re}(\lambda_n) < 0$ . We will show below these two



1 kinds of modes roughly belong to IGWs and free mode of convection, respectively. Equation (29) has  
 2 solutions in the form of  $T_n = C_n e^{\Lambda_n t}$ . By substituting the form into (29), we have

3

$$4 \quad \Lambda_n = \pm \sqrt{[-\text{Re}(\lambda_n) - f^2]^2 + [-\text{Im}^2(\lambda_n)]} e^{i \frac{\theta_n}{2}} \quad (37)$$

5

6 where

7

$$8 \quad \theta_n = \begin{cases} \arctan\left[\frac{-\text{Im}(\lambda_n)}{-\text{Re}(\lambda_n) - f^2}\right]; & \text{Re}(\lambda_n) < -f^2 \text{ (Convection)} \\ \arctan\left[\frac{-\text{Im}(\lambda_n)}{-\text{Re}(\lambda_n) - f^2}\right] + \pi; & \text{Im}(\lambda_n) > 0 \text{ and } \text{Re}(\lambda_n) > -f^2 \text{ (IGW)} \\ \arctan\left[\frac{-\text{Im}(\lambda_n)}{-\text{Re}(\lambda_n) - f^2}\right] - \pi; & \text{Im}(\lambda_n) < 0 \text{ and } \text{Re}(\lambda_n) > -f^2 \text{ (IGW)} \end{cases} \quad (38)$$

9

10 There is a simple way to determine directly the property of a mode  $\Lambda_n$ . Since  $\nabla \sigma$  is usually very small,  
 11  $\text{Im}(\lambda_n)$  is also small as compared with  $\text{Re}(\lambda_n)$ . So by letting  $\text{Im}(\lambda_n)=0$ , unstable and stable mode given  
 12 by (29) are regarded as convection and IGW mode, respectively. The existence of  $\text{Re}(\lambda_n)$   
 13  $< -f^2$  corresponds to the case of  $\sigma < 0$  in some domain of the atmosphere and can be shown as unstable  
 14 modes describing free convection. Also, modes with  $\text{Re}(\lambda_n) > -f^2$  belong to IGWs that coexisting with  
 15 modes of free convection. As  $f^2$  is relatively a small parameter, it is usually negligible.

16 For modes with  $\text{Re}(\lambda_n) < -f^2$ , it can be inferred from the relation  $I_n^{\text{positive}} < I_n^{\text{negative}}$  that strong  
 17 convective activities which can be measured by the average value of  $\|\nabla A_n\|^2 + 1/2 \text{const.}^2 \|A_n\|^2$ , are  
 18 mainly confined to the finite domain of  $\sigma < 0$ . In fact, domain of stable stratification is usually greater  
 19 than that of unstable stratification, therefore  $I_n^{\text{positive}} < I_n^{\text{negative}}$  gives

20



1

2

$$\frac{\overline{(\|\nabla A_n\|^2 + 1/2 \text{const.}^2 \|A_n\|^2)_{\Omega_{\sigma < 0}}}}{\overline{(\|\nabla A_n\|^2 + 1/2 \text{const.}^2 \|A_n\|^2)_{\Omega_{\sigma \geq 0}}}} > \frac{\Omega_{\sigma \geq 0}}{\Omega_{\sigma < 0}} \gg 1 \quad (39)$$

3

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where overbar denotes the weighted average by  $|\sigma|$  over corresponding domains. The physical meaning can be explained in a simple way that convection modes are trapped by domain of  $\Omega_{\sigma < 0}$ . Similarly, it can be shown that modes of IGWs with  $\text{Re}(\lambda_n) > 0$  coexisting with convection mode in this domain of  $\sigma < 0$  need not to be trapped and can radiate outward. A very interesting fact can be inferred from  $\text{Re}(\lambda_n)$  that IGWs become slowly-growing unstable modes in addition to oscillating and propagating as long as  $\text{Im}(\lambda_n) \neq 0$  due to  $\nabla \sigma \neq 0$ . This means IGWs need not to be generated by convective activities, but it is rather generated by the horizontal inhomogeneity of the stratification. For the same reason, convection modes in this case become slowly oscillatory in addition to rapidly growing.

Finally, the inhomogeneous part of equation (26) can be investigated by projecting (26) onto  $A_{npp}(x, y, p)$ , which gives

$$\frac{d^2 T_n}{dt^2} + (\lambda_n + f^2) T_n = R_n(t) \quad (40)$$

It describes both forced convection and the two-way interaction between convection and imbalance forcing. Also further study on the triggering of convection can employ (40) as the starting equation.

#### 4.2 Generalization for symmetric inertial instability

The results in section 4.1 can be generalized to the case of symmetric inertial instability given jointly by the equation in table I and (24) as



1

2

$$\frac{\partial^2 \bar{\delta}_{pp}}{\partial t^2} + \sigma \nabla^2 \bar{\delta} + f(f + \zeta_0) \bar{\delta}_{pp} = \bar{\mathfrak{R}}(\zeta, \varphi) \quad (41)$$

3

4

Similarly, it is easy to show convection modes are defined by eigenvalue problem as below

5

6

$$\sigma \nabla^2 A_n = [\lambda_n - f(f + \zeta_0)] A_{npp} \quad (42)$$

7

8

Some procedures analogous to those in section 4.1 give

9

$$\text{Re}(\lambda_n) = \frac{\lambda_n + \lambda_n^*}{2} = \frac{\int_{\Omega} [\sigma \|\nabla A_n\|^2 - 1/2 \|A_n\|^2 \Delta \sigma + f(f + \zeta_0) \|\partial A_n / \partial p\|] d\Omega}{\int_{\Omega} \|\partial A_n / \partial p\|^2 d\Omega} \quad (43a)$$

$$\text{Im}(\lambda_n) = \frac{\lambda_n - \lambda_n^*}{2} = \frac{\int_{\Omega} \nabla \sigma (A_n^* \nabla A_n - A_n \nabla A_n^*) d\Omega}{2 \int_{\Omega} \|\partial A_n / \partial p\|^2 d\Omega} \quad (43b)$$

12

13

One can further discuss free and forced convection mode of symmetric inertial instability based on this

14

result.

15

### 5 Meso-scale convection with horizontally uniform $\sigma$

16

The particular case of  $\sigma$  being  $p$ -dependent only in (26) will be discussed in detail in this section, not

17

only because our previous results in this case need to be modified, but also because the applications

18

become possible in the analysis of meso-scale systems such as those in tropical region where a horizontally

19

uniform unstable  $\sigma$  in lower atmosphere is a good approximation.



1 5.1 Analytical solution: convection and IGWs

2 By projecting (26) on  $P_n$ , the vertical modes defined by the eigen-system

3 
$$-\frac{d^2 P_n}{dp^2} = \lambda_n \sigma P_n; \quad n = 0, 1, 2, \dots \quad (44)$$

4 satisfying suitable lower and upper boundary conditions (Zhao *et al.*, 2011), we obtain

5 
$$\frac{\partial^2 \delta_n}{\partial t^2} - c_n^2 \nabla^2 \delta_n + f^2 \delta_n = \mathfrak{R}_n(\zeta, \varphi) \quad (45)$$

7 Here,  $c_n^2 = 1/\lambda_n$ . For stable vertical modes with  $c_n^2 > 0$ , (45) describes the IGWs and the spontaneous  
 8 emission (Lighthill, 1952; Ford *et al.*, 2000). Whereas for unstable vertical modes with  $c_n^2 < 0$ , (45)  
 9 describes convection. It may be quite common that for a stratification being unstable in some certain layer,  
 10 we have both eigenvalues of  $c_n^2 < 0$  and  $c_n^2 > 0$ , convection and IGW modes coexist in one region. An  
 11 very interesting fact can be inferred from the last section is the vertical modes of convection are trapped in  
 12 the layer of  $\sigma < 0$ , and so are modes of free and forced convection. So, actual convection comes out to be  
 13 the sum of both modes, namely

14 
$$\delta = \sum_{c_n^2 > 0} \delta_n + \sum_{c_n^2 < 0} \delta_n \quad (46)$$

16 A convection mode of  $c_n^2 < 0$  is the super position of homogeneous and inhomogeneous solutions of (45),  
 17 corresponding to free and forced convection, respectively. It is given previously by Zhao *et al.* (2011) as

18  
 19  
 20 
$$\delta_n(\mathbf{r}, t) = A_n \exp(k_x x + k_y y + \omega t) i - \frac{1}{4\pi c_n^2} \int \int \int_{t' < t}^{\infty} \mathfrak{R}_n(\mathbf{r}', t') G(\mathbf{r} - \mathbf{r}', t - t') d\mathbf{r}' dt' \quad (47)$$



1

2

3 The growth rate of the free unstable mode is obtained from the dispersion relation as

4  $\lambda = i\omega = \sqrt{-(k_x^2 + k_y^2)c_n^2 - f^2}$ , while forced convection are given by the Green's function

$$5 \quad G(\mathbf{r}, \mathbf{r}', t, t') = \frac{1}{4\pi} \frac{\exp[i \frac{f}{\sqrt{-c_n^2}} \sqrt{|\mathbf{r} - \mathbf{r}'|^2 - c_n^2(t-t')^2}]}{\sqrt{|\mathbf{r} - \mathbf{r}'|^2 - c_n^2(t-t')^2}} \quad (48)$$

6

7 where  $\mathbf{r} = x\mathbf{i} + y\mathbf{j}$ , and the causality demands  $t > t'$ . Rather than just these portions were considered

8 previously, IGW modes of  $c_n^2 > 0$  also need to be considered in this paper as the superposition of its free

9 IGW mode (homogeneous solution) and spontaneous emission of IGW (inhomogeneous solutions). Unlike

10 free modes of convection, free modes of IGW are stable and unable to grow, so we just need to consider the

11 spontaneous emission of IGW which is given by

12

$$13 \quad \delta_n(\mathbf{r}, t) = \frac{c_n^2}{4\pi} \int_{c_n(t-t') > |\mathbf{r}|} \iint_{\Omega} \Re(\mathbf{r}', t') G(\mathbf{r} - \mathbf{r}', t - t') d\mathbf{r}' dt' \quad (49)$$

14 where the Green's function  $G$  is (see Appendix C)

15

$$16 \quad G(\mathbf{r} - \mathbf{r}', t - t') = \begin{cases} \frac{c_n^2}{4\pi} \frac{\exp[i \frac{f}{c_n^2} \sqrt{c_n^2(t-t')^2 - |\mathbf{r} - \mathbf{r}'|^2}]}{\sqrt{c_n^2(t-t')^2 - |\mathbf{r} - \mathbf{r}'|^2}}, & |\mathbf{r} - \mathbf{r}'| < c_n(t-t') \\ \frac{c_n^2}{4\pi i} \frac{\exp[-\frac{f}{c_n^2} \sqrt{|\mathbf{r} - \mathbf{r}'|^2 - c_n^2(t-t')^2}]}{\sqrt{|\mathbf{r} - \mathbf{r}'|^2 - c_n^2(t-t')^2}}, & |\mathbf{r} - \mathbf{r}'| > c_n(t-t') \end{cases} \quad (50)$$

17





1 Here  $\Omega$  denotes the integrating domain  $|\mathbf{r}-\mathbf{r}'|<c_n(t-t')$ . The Green's function in domain  
 2  $|\mathbf{r}-\mathbf{r}'|>c_n(t-t')$  remains imaginary and has no contribution to the field of divergence. The physical  
 3 meaning is explained as the amplitude of IGW at time  $t$  in place  $\mathbf{r}$  is decided by the accumulation of the  
 4 forcing effect at all the earlier time  $t'$  in everywhere  $\mathbf{r}'$ . If  $|\mathbf{r}-\mathbf{r}'|=c_n(t-t')$  is viewed as the pure wave  
 5 front of IGW, (49) indicates that its influence is inversely proportional to the distance between  $\mathbf{r}$  and the  
 6 wave front. Moreover, the influence of the wave front at  $\mathbf{r}$  after it overtakes this point is mainly inertial  
 7 oscillation, while it has no influence before the overtaking. Overall, IGW behaves primarily as the  
 8 disturbance around the wave front.

### 9 *5.2 Deep structures of convective activities inside and outside meso-scale system*

10 The analytical inhomogeneous solutions of our studies seem too complicate in form to have practical  
 11 use. Nevertheless, they have approximate forms that are applicable for the straightforward estimation of  
 12 convection/IGW structures inside and outside a meso-scale system as follows.

13 Inside the meso-scale imbalanced vortical flow region, the Froude number  $Fr$  for a meso-scale system  
 14 can be estimated by  $Fr=U/\sqrt{gH}$ .  $U\sim 10^1 m/s$  and  $H\sim 10^4 m$  are the wind scale and vertical scale,  
 15 respectively. So we have  $Fr\ll 1$  and can demand  $Fr\propto U/c_n\ll 1$  in (45), which confines the present  
 16 discussion to the deep structure of meso-scale convection system. We have also the Rossby number  
 17  $Re=O(1)$ , and let  $L$  be the scale of the imbalance of meso-scale system, thus a comparison between the  
 18 magnitudes of different terms of the left side hand of (45) gives

19  
 20 
$$\frac{\partial^2/\partial t^2}{c_n^2\nabla^2}\propto\frac{1/T^2}{c_n^2/L^2}=\frac{U^2}{c_n^2}=Fr^2\ll 1 \quad (51a)$$

21 
$$\frac{f^2}{c_n^2\nabla^2}=\frac{f^2}{c_n^2/L^2}=\left(\frac{Fr}{Re}\right)^2\ll 1 \quad (51b)$$

22



1 As a result, (45) becomes

2

3

$$-c_n^2 \nabla^2 \delta_n \approx \mathfrak{R}_n(\zeta, \varphi) \quad (52)$$

4

5 Since both forced convection modes with  $c_n^2 < 0$  and IGW modes with  $c_n^2 > 0$  contribute to the  
 6 convergence or the vertical motion, they should be viewed as the components of convection. The structure  
 7 of deep convection inside the meso-scale system can be estimated simply by

8

$$\delta_n \propto -\nabla^2 \delta_n \propto \begin{cases} \mathfrak{R}_n(\zeta, \varphi) / c_n^2, & c_n^2 > 0 \\ -\mathfrak{R}_n(\zeta, \varphi) / c_i^2, & c_n^2 = -c_i^2 < 0 \end{cases} \quad (53)$$

10

11

12 Anyway, this structure just applies to forced convection. As an example to illustrate convective responses  
 13 that the (53) would predict, we consider an idealized system with a moving upper-level disturbance. A  
 14 moving upper-level disturbance can result in vorticity or temperature advection, which is an imbalance  
 15 forcing. After projected onto vertical modes, the forced modes of convection and IGW are estimated by the  
 16 structures of such imbalance forcing according to (53). Although forced IGW modes contribute also to  
 17 vertical motion, an essential difference is that forced convection modes are trapped in the unstable layer of  
 18 stratification. In addition, free modes of convection contribute to the spatial scales of the convective  
 19 activities as well. They tend to select the smallest scales to develop and are embedded in the forced  
 20 convection.

21 Outside the meso-scale system, forced convection/IGWs with scales much larger are always induced. As  
 22 was suggested by Ford (2000), the imbalance forcing is confined to a meso-scale region with diameter  $L$ . If  
 23 wind speed scale is  $U$ , then that of temporal variations is  $L/U$ . So growth rate of the free mode of



1 convection with wavenumber  $k$  can be estimated by the dispersion relationship, i.e.  $\lambda = \sqrt{c_i^2 k^2 - f^2}$ , while  
 2 the frequency of the free mode of inertia-gravity waves can be estimated by  $\omega = \sqrt{c_n^2 k^2 + f^2}$ . We can  
 3 assume both of them are proportional to  $L/U$ , namely the time scale of the variation of the vortical flow as  
 4 the source of forcing. So the scale of forced convection as well as IGWs outside the meso-scale system is  
 5  $2\pi L / Fr \gg L$  when  $Fr \ll 1$ . As suggested by the Green's function of forced convection and IGWs, these  
 6 structures may move toward and outward the source of forcing, respectively (Zhao et al 2010; 2011).

### 7 5.3 Approximate horizontal structure outside a meso-scale system

8

9 The form of Green function solution in section 5.1 can be transformed into an easier way to estimate the  
 10 structure outside a meso-scale system. The structure of imbalance forcing  $\mathfrak{R}(\zeta, \varphi)$  might be very complex.  
 11 In order to reflect the influence of such asymmetry of  $\mathfrak{R}(\zeta, \varphi)$  over the outside region of the meso-scale  
 12 system, it is convenient to introduce its multipole description such as monopole, dipole and quadrupole as

13

$$14 \quad m(t') = \iint_D \mathfrak{R}_n(\mathbf{r}', t') dS \quad (54a)$$

$$15 \quad \mathbf{p}(t') = \iint_D \mathfrak{R}_n(\mathbf{r}', t') \mathbf{r}' dS \quad (54b)$$

$$16 \quad \tilde{\mathbf{q}}(t') = \iint_D \mathfrak{R}_n(\mathbf{r}', t') \mathbf{r}' \mathbf{r}' dS \quad (54c)$$

17

18 respectively. Here,  $D$  is the area covered by system and  $\mathbf{r}'$  is a point within it. They are all functions of time  
 19  $t'$ . Suppose Green's function is  $G(\mathbf{r} - \mathbf{r}', t - t')$ , so the forced solution of (45) with  $\mathbf{r}$  far from  $D$  or  
 20  $\|\mathbf{r}'\|/\|\mathbf{r}\| \propto Fr \ll 1$  at any time  $t$  can be approximated by multipole expansion

21

$$22 \quad \begin{aligned} \delta_n(\mathbf{r}, t) &= \int \iint_{t>t', D} \mathfrak{R}_n(\mathbf{r}', t') G(\mathbf{r} - \mathbf{r}', t - t') d\mathbf{r}' dt' \\ &= \int_{t>t'} [m(t') G_0(\mathbf{r}, t - t') - \mathbf{r} \cdot \mathbf{p}(t') G_1(\mathbf{r}, t - t') + \mathbf{r} \mathbf{r} : \tilde{\mathbf{q}}(t') G_2(\mathbf{r}, t - t') + \dots] dt' \quad (55) \end{aligned}$$



1

2 Here,  $G_0$ ,  $G_1$ ,  $G_2$  and *etc.* are determined by  $G$  and their forms are not given here for the simplicity. As a  
3 result, the far-field response at  $O(1)$ ,  $O(F_r)$  and  $O(F_r^2)$  are determined by  $m(t')$ ,  $\mathbf{p}(t')$  and  $\bar{\mathbf{q}}(t')$ ,  
4 respectively. If strong imbalance comes out for some reason, this imbalance will cause far-field IGW and  
5 convection  $\delta_n(\mathbf{r}, t)$  as nearly free wave, whose dispersion tends to weaken itself, i.e.  $\delta_n(\mathbf{r}, t) \rightarrow 0$  as  $t$   
6  $\rightarrow \infty$ . The only way for that is  $\Re(\zeta, \varphi) \rightarrow 0$  as  $t \rightarrow \infty$ . So it tends to remove imbalance on the contrary.  
7 This is known as the process of balanced flow adjustment. The compromise between these two tendencies  
8 of generating and reducing of imbalance turns out to keep the imbalance and its radiation given mainly by  
9 the quadrupole radiation (Ford, 2000). So, lower order monopole or even dipole imbalance will be  
10 eliminated immediately by the process of balanced flow adjustment. This fact can be useful in the  
11 understanding regarding some of typhoon's behaviors in the next section.

12

### 13 **6 Typhoon properties as an example of potential application**

14 For the purpose of application, we need to know the physical meaning of the imbalance forcing  $\Re(\zeta, \varphi)$   
15 in (3). This imbalance forcing has something to do with the spatio-temporal inhomogeneities of the basic  
16 flow, which are called systems by meteorologists. Thus it may be viewed as a forcing upon convection by  
17 meso-scale system. The term  $\Re(\zeta, \varphi)$  is also closely related to the process of the adjustment of  
18 geostrophic and gradient flows as was discussed in the end of the last section. If the vertical or horizontal  
19 structures of the terms in brackets in  $\Re(\zeta, \varphi)$  are approximately sine or cosine functions, the imbalance  
20 forcing can be roughly replaced by the terms of  $(a_\zeta^2 + b_\zeta^2 - \zeta^2)_i$  (nonsteady processes of the vortical flow),  
21  $\mathbf{V}_\zeta \cdot \nabla \zeta$  (vorticity advection by the vortical part of the flow) and  $[\mathbf{V}_\zeta \cdot \nabla (\frac{\partial \varphi}{\partial p})]_p = -[\mathbf{V}_\zeta \cdot \nabla \nu]_p$  (difference of  
22 specific volume  $\nu$  advectons by the vortical flow between upper and lower levels). Notice that a constant  
23 background wind field has been absorbed into the vortical part of the flow  $\mathbf{V}_\zeta$ .



1 Usually, study on meso-scale convection stresses the role of water vapor and condensation. Emanuel et  
 2 al.(1994) argue that the overall effect of moist or diabatic convection on larger-scale circulations can be  
 3 viewed just as a reduction (by roughly an order of magnitude) to the effective static stability of such  
 4 circulations. Similarly, since our framework applies to meso-scale convective activity rather than small  
 5 scale cells as is mentioned in section 2, in the following case of typhoon, as a meso- $\alpha$ -scale system, we can  
 6 assume a horizontally-averaged water vapor distribution  $\bar{q}(p)$ , which is steady in time but changes with  
 7 height. The condensation heating is assumed as  $Q_c = -L \frac{\partial \bar{q}}{\partial p} \omega$ . By substituting it into thermodynamic  
 8 equation (A1c) in Appendix A (i.e.  $\frac{\partial}{\partial t}(\frac{\partial \varphi}{\partial p}) = -\sigma \omega - \mathbf{V} \cdot \nabla(\frac{\partial \varphi}{\partial p})$ ), we obtain an effective static stability  
 9 parameter  $\sigma_e = \sigma - \frac{LR}{c_p p} \frac{\partial \bar{q}}{\partial p}$ . So we can introduce an effective static stability to reflect roughly the effect  
 10 of moist or diabatic convection, and above discussion seems unchanged in form. Therefore, the concept of  
 11 imbalance forcing of both convection and IGWs, or more accurately the interaction between imbalanced  
 12 vortical flow and convection/IGW modes, has potential applications in many aspects of meso-scale systems  
 13 with or without moisture.

14 As a simple example of application, this theory may be supportive in understanding some key issues of  
 15 typhoon study such as typhoon's organization and the relationship between typhoon recurvature (a sudden  
 16 turning of typhoon track, see *e.g.* Chen et al, 2002) and typhoon's asymmetric structure. The change of  
 17 meso-scale disturbances associated with typhoon is usually owed to linear barotropic instability or linear  
 18 inertial instability. See, *e.g.* Hendricks et al. (2009) for barotropic instability and Vigh and Schubert (2009)  
 19 for inertial instability. However, as was argued above, any mention of instability implies there is a  
 20 prescribed and balanced axisymmetric basic flow under the present circumstance, which excludes more  
 21 possibilities associated with the two-way interaction between convection/IGW and imbalanced basic state  
 22 of typhoon. In fact, it's difficult in real atmosphere to have a strict balanced axisymmetric solution ( $\zeta_0, \varphi_0$ )  
 23 as the basic state for a typhoon, due to its moving with shear flows, asymmetric latent and sensible heating,



1 the presence of surface friction,  $\beta$ -effect and *etc.* As a result, the imbalance forcing  $\Re(\zeta, \varphi)$  needs not to  
2 vanish and its structure may be also asymmetric. So, the multipole description of far-field effects of  
3  $\Re(\zeta, \varphi)$  and the balanced flow adjustment theory of these multipoles stated in section 5.3 seem to be  
4 useful for this purpose of further studies in application, such as issues of typhoon as below.

5 1) Typhoon's self-organization

6 Balanced flow adjustment theory of multipole description of imbalance can play an important role in the  
7 process of typhoon's self-organization. First of all, an idealized mature typhoon tends to a balanced basic  
8 flow which is steady in time and have a dynamically and thermo-dynamically axisymmetric structure. This  
9 means there is no imbalance forcing and their multipoles due to  $(a_\zeta^2 + b_\zeta^2 - \zeta^2)_t = 0$ ,  $\mathbf{V}_\zeta \cdot \nabla \zeta = 0$  as well as  
10  $[\mathbf{V}_\zeta \cdot \nabla v]_p = 0$  everywhere. However, for a small, but finite amplitude tropical disturbance, processes that  
11 have been established to be essential elements in the self-organization of typhoon are moist convective  
12 instability, vortical hot tower formation, vorticity aggregation and sea-to-air moisture exchange (see, e.g.,  
13 Montgomery and Smith, 2014). Accompanied with these processes before a mature typhoon is finally  
14 formed, the disturbance may have a strong imbalance due to the unsteady and asymmetric natures of  
15 vortical flow of the disturbance. Such imbalance will produce forced modes of IGW/convection radiating  
16 outwards and then give rise to balanced flow adjustment which diminishes the unsteady and asymmetric  
17 imbalance natures of vortical flow and adjusts toward a steady and axisymmetric structure. So balanced  
18 flow adjustment must be considered as another possible element in the self-organization of typhoon. Its key  
19 role is to help other processes mentioned above attain an axisymmetric balance among them. This is even  
20 more clearly seen and can be applied to the explanation of the self-organization process of typhoon's  
21 structure as follows. If we write  $\zeta$  (or  $a_\zeta$  and  $b_\zeta$ ) of the disturbance in polar coordinates  $(r, \theta)$  with the  
22 typhoon center being the origin of the coordinate system and expand in Fourier series

23

24 
$$\zeta(r, \theta, t) = \zeta_0(r, t) + \zeta_1(r, t)e^{i\theta} + \zeta_2(r, t)e^{i2\theta} + \dots \quad (57)$$



1

2 These three terms are associated with the rotational monopole, dipole and quadrupole structures of  $\zeta$  in  
 3 typhoon, respectively. However, they need not to be consistent with those of enstrophy  $\zeta^2$ , because it can be  
 4 shown that  $\zeta^2$  has the following form

5

$$6 \quad \zeta^2 = \zeta\zeta^* = (\zeta_0^2 + \zeta_1^2 + \zeta_2^2) + d(\zeta_0, \zeta_1, \zeta_2) \cos[\theta - \theta_d(\zeta_0, \zeta_1, \zeta_2)] + q(\zeta_0, \zeta_2) \cos 2[\theta - \theta_q(\zeta_0, \zeta_2)] + \dots \quad (58)$$

7

8 Here,  $d$  and  $\theta_d$  describe the magnitude and phase of the dipole, respectively, while  $q$  and  $\theta_q$  the quadrupole.  
 9 These three parties in (58) are associated with monopole, dipole and quadrupole structures of enstrophy  $\zeta^2$ ,  
 10 respectively. The self-organization process is thus related to the adjustment to remove the tendencies of  
 11 monopole, dipole and even quadrupole of enstrophy  $\zeta^2$  (or  $a_\zeta^2 + b_\zeta^2$ ). So we have roughly  
 12  $(\zeta_0^2 + \zeta_1^2 + \zeta_2^2)_t \rightarrow 0$ ,  $d(\zeta_0, \zeta_1, \zeta_2)_t \rightarrow 0$  and  $q(\zeta_0, \zeta_2)_t \rightarrow 0$ , whose solution is  $(\zeta_0, \zeta_1, \zeta_2) \rightarrow const$ . This  
 13 does not need to remove the monopole, rotational dipole and quadrupole of typhoon associated with  $\zeta_0$ ,  $\zeta_1$   
 14 and  $\zeta_2$ , although there may be enstrophy exchange among them. On the other hand, the balanced flow  
 15 adjustment tends also to remove the imbalance caused by  $\mathbf{V}_\zeta \cdot \nabla \zeta \neq 0$ . As mentioned in above,  $\mathbf{V}_\zeta \cdot \nabla \zeta$   
 16 and its multipoles vanishes for an axisymmetric structure. So imbalance of  $\mathbf{V}_\zeta \cdot \nabla \zeta \neq 0$  and its multipoles  
 17 are due to the asymmetric structure of  $\zeta$  of the disturbance. The balanced flow adjustment then tends to  
 18 suppress the asymmetric portion such as  $\zeta_1$  and  $\zeta_2$  to develop further and allow axisymmetric structure  $\zeta_0$   
 19 to grow up for a longer time. This is also the case for the axisymmetric thermodynamical structure  
 20 formation of height or temperature related to  $[\mathbf{V}_\zeta \cdot \nabla v]_p$ . The corresponding observations stated by  
 21 Montgomery and Smith (2014) are as below. Since the process of spin-up is similar in almost all processes  
 22 known to be necessary for self-organization mentioned in above, involving the convectively-induced  
 23 inflow in the lower troposphere, which draws in absolute angular momentum surfaces to amplify the  
 24 tangential wind component. So the fact that these processes tend to select the axisymmetric component of



1 the disturbance to strengthen is attributed to the tendency of balanced flow adjustment to suppress  
2 asymmetry. When  $(\cdot)_t \rightarrow 0$  the finally-attained magnitude of  $\zeta_0$  is relatively larger than those of  $\zeta_1$ ,  $\zeta_2$   
3 and *etc.*, so a mature typhoon usually has a roughly axisymmetric basic structure and the dependence of  $\zeta_0$   
4 on  $r$  determine the intensity and size of typhoon. The self-organization of typhoon and its convective  
5 activity is then accomplished. Since balanced flow adjustment cannot reduce imbalance completely, a real  
6 typhoon cannot be axisymmetric exactly, and dipole and quadrupole or even higher order multipole of  
7 vorticity and deformation can exist as well, for which the existence of typhoon's spiral rainband may be  
8 viewed as the evidence.

9

## 10 2) Mechanism of Fujiwhara effect

11 The Fujiwhara effect (Fujiwhara,1921) is following phenomena observed when two typhoons are in  
12 proximity of one other. a) Their centers will begin orbiting cyclonically about a point between the two  
13 typhoons. b)The two typhoons will be attracted to each other and c) eventually spiral into the center point  
14 and merge. It has not been agreed upon whether this is due to the divergent portion of the wind or vorticity  
15 advection (DeMaria and Chan, 1984).

16 The mechanism of these phenomena can be again attributed to a process similar to that of typhoon's  
17 self-organization in above. When two typhoons with almost equal size and intensity come close to each  
18 other, they begin providing steering flow to each other and orbiting cyclonically about a point between the  
19 two systems. If interaction between them are considered, they can be viewed as one single super typhoon  
20 system with its center located at orbiting center between the two typhoons. The key point to consider such  
21 issues is that the interaction between two nearly balanced typhoons can generate imbalance, while balanced  
22 flow adjustment tends to select the way with a imbalance as weak as possible and will finally lead to a new  
23 balance. Although analysis in analogy with that for self-organization in above can predict the result that  
24 two typhoons may eventually merge into one single typhoon or phenomenon c), the details of process of





1 such adjustment are still necessary to explain phenomena mentioned previously. If orbiting center between  
2 the two typhoons is chosen as the origin of the coordinate system, we can use (57) to describe the super  
3 typhoon system. Notice  $\zeta_1=0$  in this case, so the adjustment to remove the tendencies of monopole and  
4 quadrupole of enstrophy  $\zeta^2$  demands  $(\zeta_0^2 + \zeta_2^2)_t \rightarrow 0$  and  $q(\zeta_0, \zeta_2)_t \rightarrow 0$ , which determines a structure  
5  $(\zeta_0, \zeta_2) \rightarrow const$ . It doesn't need to mean one single typhoon can be formed before we are sure  $\zeta_2$   
6 diminishes essentially due to the adjustment to remove  $\mathbf{V}_\zeta \cdot \nabla \zeta$ , which will be demonstrated physically  
7 as below by figure 1. Cyclonically orbiting of the two typhoons about the origin  $o$  may cause positive  
8 (negative) vorticity advection in front of (behind) each single typhoon with respect to the directions of their  
9 motions. While in a Cartesian coordinate system, this distribution of vorticity advection has central  
10 antisymmetric structure, i.e. the values of vorticity advection at  $(x, y)$  and  $(-x, -y)$  are the same, and  
11 meanwhile it is also symmetric about two axes. So both monopole and dipole of vorticity advection vanish,  
12 and primarily a quadrupole structure appears. Usually among monopole, dipole and quadrupole structures  
13 of vorticity advection, quadrupole structure of vorticity advection produce relatively a weakest imbalance,  
14 so the manner of interaction in a) which produce only quadrupole structure of vorticity advection is  
15 selected as the way of interaction.. The magnitude of the quadrupole structure is proportional to both the  
16 strength of vorticity advection regions and to the distance between a advection regions and the origin. The  
17 former depends highly on the intensity of typhoons, while the latter the distance between two centers of  
18 typhoons. Suppose the intensity of two typhoons remains almost unchanged, the balanced flow adjustment  
19 tends to decrease the magnitude of the quadrupole of vorticity advection by reducing the distance between  
20 two centers of typhoons, until it becomes zero and one single typhoon forms. This gives reasonable  
21 explanations to phenomenon b) and c).

22

23 3) Asymmetry of typhoon and its motion

24 Imbalance forcing is also associated with vorticity advection by the vortical flow, namely,  $\mathbf{V}_\zeta \cdot \nabla \zeta$ . Here,



1 a spatially uniform but time-dependent background wind field has been absorbed into  $\mathbf{V}_\zeta$ , which can be  
 2 selected as the wind speed of the center of typhoon and denoted by  $\mathbf{V}_0(t)$ . So

3

$$4 \quad \mathbf{V}_\zeta = \mathbf{V}_0(t) + \mathbf{V}'_\zeta \quad (59)$$

5

6 here  $\zeta = \nabla \times \mathbf{V}'_\zeta$ . Thus, the monopole of the vorticity advection is given by

7

$$8 \quad m(t') = \iint_D \mathbf{V}_\zeta \cdot \nabla \zeta dS \propto \mathbf{V}_0(t) \cdot \overline{\nabla \zeta} + \overline{\mathbf{V}'_\zeta \cdot \nabla \zeta} = \|\mathbf{V}_0(t)\| \|\overline{\nabla \zeta}\| \cos \alpha \quad (60)$$

9 Hereafter, “ $\overline{\quad}$ ” denotes  $(1/D) \iint_D (\cdot) dS$ . And  $\alpha$  is the angle between the direction of typhoon movement

10 and the averaged vorticity gradient  $\overline{\nabla \zeta}$ . Here, notice also  $\overline{\mathbf{V}'_\zeta \cdot \nabla \zeta} = \overline{\nabla \cdot (\mathbf{V}'_\zeta \zeta)} - \zeta \overline{\nabla \cdot \mathbf{V}'_\zeta} = \overline{\nabla \cdot (\mathbf{V}'_\zeta \zeta)} = 0$ , if we

11 assume there is no net flux  $\zeta \mathbf{V}'_\zeta$  into the area  $D$  covered by typhoon through its edge. Suppose  $\|\mathbf{V}_0(t)\|$  and

12  $\|\overline{\nabla \zeta}\|$  are nearly constant, we have largest values of imbalance where  $\alpha = 0$  or  $\pi$ , and smallest value of 0

13 where  $\alpha = \pi/2$  or  $-\pi/2$ . Notice also that we have  $\overline{\nabla \zeta} = 0$  for an exactly axisymmetric typhoon. If the

14 structure of typhoon becomes asymmetric *i.e.*  $\overline{\nabla \zeta} \neq 0$  for some reason and there is a value  $\alpha$  far enough

15 from  $\pm \pi/2$  (quite often near to 0 or  $\pi$  in observations, as will be shown subsequently), then strong

16 monopole of imbalance caused by vorticity advection comes out. According our previous discussions, the

17 balanced flow adjustment tends to eliminate this monopole part of imbalance immediately by adjusting  $\alpha$

18 toward the nearer one of  $\alpha = \pi/2$  and  $-\pi/2$ . Usually this process of balanced flow adjustment may be

19 accompanied with the turning of  $\mathbf{V}_0(t)$  or typhoon recurvature. Such issue is also proposed as the effect of

20 interaction of typhoon with a steering flow upon typhoon track. If one decomposes  $\overline{\nabla \zeta}$  into  $\overline{\nabla \zeta_s}$  a

21 portion from steering flow, and  $\overline{\nabla \zeta_T}$  a portion from typhoon. It is easy to see that we have both  $\overline{\nabla \zeta_s} = 0$

22 and  $\overline{\nabla \zeta_T} = 0$  for an axisymmetric typhoon in a uniform steering flow, so typhoon will just move with

23 steering flow and no change of typhoon track can happen. Furthermore, if one assumes typhoon as an



1 axisymmetric component of the stream, then  $\overline{\nabla \zeta_T} = 0$ , and averaged vorticity gradient is mainly from  
 2 steering flow. In the latter case, previous research (see, *e.g.* Kasahara and Platzman, 1963; Demaria 1985)  
 3 find that vorticity gradient of steering flow results in a component of motion  $\pi/2$  to the left of the gradient,  
 4 together with a component in the direction of the gradient. On the contrary, in the case of weak steering  
 5 flow, which means both uniform component  $\overline{U_s}$  and  $\overline{\nabla \zeta_s}$  of shear component are negligible for it, and  
 6  $\overline{\nabla \zeta} \approx \overline{\nabla \zeta_T}$ , it is summed up from observations that there are four categories of asymmetric structure of the  
 7 typhoon that may be connected to typhoon recurvature in Chen et al. (2002). Upon their figures of observed  
 8 stream fields indicated in figure 2, we mark the averaged vorticity gradient  $\overline{\nabla \zeta}$  and the observed turning of  
 9 typhoon track by arrows in blue dashed line and red solid line, respectively. Our theory can give quite  
 10 reasonable explanation to this connection in all above cases. If we regard typhoons in figure 2 are  
 11 axisymmetric and asymmetries are from a weak steering flow with  $\overline{U_s} \approx 0$  and  $\overline{\nabla \zeta_s} \neq 0$ , we have  
 12  $\overline{\nabla \zeta} \approx \overline{\nabla \zeta_s}$  and conclusions remain the same, while turning of typhoon track is attributed to steering flow,  
 13 which can be another point of view. The results in Demaria (1985) may have different mechanism, because  
 14 a non-divergent barotropic model is employed and  $\beta$ -effect is considered.

15 Similarly, thermo-dynamical asymmetric structure of typhoon which may be caused by its dynamics and  
 16 by latent heat release as well as the distribution of low-boundary heating such as SST(sea surface  
 17 temperature), may also affect typhoon track. Because the difference of temperature or specific volume  $v$   
 18 advections by the vortical flow between upper and lower levels gives also imbalance forcing, it can be  
 19 shown that

20

$$21 \quad m(t') = \iint_D [\mathbf{V}'_\zeta \cdot \nabla v]_p dS \propto -[\|\mathbf{V}_0\| \|\overline{\nabla v}\| \cos \beta]_p \quad (61)$$

22

23 In the derivation,  $\overline{\mathbf{V}'_\zeta \cdot \nabla v} = \overline{\nabla \cdot (\mathbf{V}'_\zeta v)} - \overline{v \nabla \cdot \mathbf{V}'_\zeta} = \overline{\nabla \cdot (\mathbf{V}'_\zeta v)} = 0$  because we assume again there is no net flux  
 24  $v \mathbf{V}'_\zeta$  into  $D$  through it edge.  $\beta$  is the angle between the moving direction of typhoon and  $\overline{\nabla v}$  the



1 averaged specific volume gradient. If heating of upper atmosphere is weak, the structure of  $v$  is  
2 approximately axisymmetric and  $\overline{\nabla v} = 0$ , then we just need to consider the value of  $\|\mathbf{V}_0\| \|\overline{\nabla v}\| \cos \beta$  at  
3 lower atmosphere. So if typhoon track intersects the contour lines of  $v$  or temperature, then there is  
4 imbalance forcing. Again, the balanced flow adjustment tends to adjust  $\beta$  toward  $\pi/2$  or  $-\pi/2$  so as to  
5 weaken this imbalance. As a result, this process is accompanied with the tendency of the typhoon track  
6 change. This can probably be used to explain how SST distribution affect typhoon track. Many researchers  
7 stated in Chen et al. (2002) notice that a typhoon passing close to a warm sea region experiences some  
8 deflection toward the warm sea region. Other researchers such as Jing (1996) also observed that typhoon  
9 tends to move along the SST contour lines of the outside edge of a warm sea region. There seems so far no  
10 good way to incorporate these two phenomena into giving a self-consistent explanation. We suppose these  
11 facts can be simply explained as below. As is shown in figure 3, the red solid line with arrow represents the  
12 track of a typhoon approaching a warm sea region. The distribution of SST around a warm sea region may  
13 cause an averaged gradient of latent heating in the lower atmosphere due to evaporation and sensible  
14 heating ones pointing to warm side of SST.

15 Typhoon may be sustained by latent heating, so the stronger latent heating in the warmer side enhances  
16 warmer side of typhoon. As a result, a tendency appears to pull typhoon toward the warmer side of SST.  
17 Meanwhile, it also implies that warmer side of typhoon has higher temperature and humidity in lower  
18 atmosphere, and  $\overline{\nabla v} \propto \nabla SST$  is a good approximation. In the early stage to approach warm SST region,  
19 typhoon track intersects the contour lines (dark thin line) of SST at a large angle and induces an imbalance  
20 to the vortical flow of typhoon. Consequently, balanced flow adjustment tends to get rid of this imbalance  
21 by compelling typhoon track to follow the SST contour lines around a warm sea region.

22 The averaged vorticity gradient and temperature gradient can change typhoon track jointly, although we  
23 discuss them independently so far. Then a question arises: which one is more important or effective to the  
24 change of typhoon track? Since vorticity gradient is usually caused by dynamical process and varies more



1 rapidly than temperature gradient that is caused mainly by thermo-dynamical process associated with  
2 heating, we suppose vorticity gradient may be relatively important or effective in altering the moving  
3 direction of typhoon. Another issue is that typhoon may have both apparent instability process and  
4 adjustment process associated with imbalance of basic flow. However, as discussed in section 3, at least  
5 linear apparent instability cannot react on the imbalanced basic flow ( $\zeta$ ,  $\varphi$ ) defined in this study and is thus  
6 almost not involved in adjustment process. It is also necessary to point out that one should be careful in  
7 explaining the dynamics of vortex motion on a  $\beta$ -plane by above theory, because the theory so far is still  
8 limited to  $f$ -plane.

## 10 **7 Summary and conclusions**

11 In the study of the convective activities of a meso-scale system, there is a big contradiction between the  
12 aspiration to apply classic theory of instabilities and the unsatisfactory conditions of these theories due to  
13 highly imbalanced natures of the basic states. By introducing an appropriately-defined imbalanced vortical  
14 flow as the basic state, our previous study in Zhao, et al (2011) has extended instability theories from  
15 balanced to imbalanced flows. This revised theory of instability considers not only the apparent instability  
16 of the imbalanced basic state but also the two-way interaction between the convective activities and this  
17 imbalanced basic state. In the linear sense, it is argued that convection can be regarded as the superposition  
18 of free modes of convection and the response to the forcing induced by the imbalance of the basic flow.  
19 Although the free modes of convection cannot act on the basic state, the forced part of convection do have  
20 a reaction on the basic state though balanced flow adjustment and prevent it's imbalance from further  
21 increase. Within the framework above, this paper makes progress in following key issues that we failed to  
22 cope with previously.

23 Firstly, we have a further insight into the triggering mechanism of convection. A study by regular  
24 perturbation method on the nonlinear case is performed for that purpose. It can be concluded that



1 convection can be triggered in resonance either with imbalance forcing of basic state or with nonlinear  
2 interaction among different modes of IGWs. Even if all these cannot happen, an imbalance forcing with  
3 strong enough magnitude may eventually trigger convection after a time delay. These are essentially  
4 different from the concept of Liyapunov instability in which an initial disturbance is necessary. So,  
5 convection is more appropriately to be regarded as a spontaneous phenomenon without external initial  
6 disturbance.

7 Secondly, in some simplified but relatively general dynamical setting for meso-scale system, the  
8 influences of the inhomogeneity of stratification on convection and IGWs are explored. Qualitative  
9 properties of free and forced modes of convection/IGW are investigated via an eigenvalue problem for  
10 arbitrarily distributed stratification. It is found that modes of convection are trapped by domain of  $\sigma < 0$ , or  
11 unstable stratification, while modes of IGWs coexisting with convection mode in this domain need not to  
12 be trapped and can propagate through or radiate outward. *And due to horizontal inhomogeneity of the*  
13 *stratification*, IGWs become slowly-growing unstable modes, in addition to oscillating and propagating,  
14 and convection modes in this case become slowly oscillatory, in addition to rapidly growing. The specific  
15 situation of horizontally uniform stratification which we considered previously in Zhao, et al. (2011) is  
16 improved. Rather than just giving forced convection mode, all vertical motions that may contribute to the  
17 structure of convection in meso-scale system are discussed, including those caused by free modes of  
18 instabilities, forced convection and IGWs. The approximate forms that are applicable for the  
19 straightforward estimation of convection/IGW structures inside and outside a meso-scale system are  
20 derived. Particularly, a multi-pole description such as monopole, dipole and quadrupole is introduced to  
21 link the induced far-field convection/IGW structures and the balanced flow adjustment inside a meso-scale  
22 system, which is useful in our subsequent study on typhoon.

23 Finally, as a simple example to demonstrate the potential application of our theory on interaction  
24 between convection/IGWs and its imbalanced basic state, the multi-pole description of imbalance forcing



1 and then balanced flow adjustment, the central idea of our theory, gives reasonable explanations to key  
 2 issues in typhoon study such as the role of balanced flow adjustment in typhoon's self-organization,  
 3 Fujiwhara effect and the influence of typhoon's asymmetric structure on its track of motion.

4

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 8 author on issues concerning typhoon track.

9

## 10 **Appendix A**

11 The basic equation are the vorticity equation, divergence equation and thermodynamic equation in  
 12  $p$ -coordinates as below

$$13 \quad \frac{\partial \zeta}{\partial t} = -f\delta - \mathbf{V} \cdot \nabla \zeta - \omega \frac{\partial \zeta}{\partial p} - \zeta \delta + \mathbf{k} \cdot \left( \frac{\partial \mathbf{V}}{\partial p} \times \nabla \omega \right) \quad (\text{A1a})$$

$$14 \quad \frac{\partial \delta}{\partial t} = f\zeta - \nabla^2 \varphi - \mathbf{V} \cdot \nabla \delta - \omega \frac{\partial \delta}{\partial p} - \frac{1}{2} (\delta^2 + a^2 + b^2 - \zeta^2) - \frac{\partial \mathbf{V}}{\partial p} \cdot \nabla \omega \quad (\text{A1b})$$

$$15 \quad \frac{\partial}{\partial t} \left( \frac{\partial \varphi}{\partial p} \right) = -\sigma \omega - \mathbf{V} \cdot \nabla \left( \frac{\partial \varphi}{\partial p} \right) \quad (\text{A1c})$$

16

17 Variables here have the same meanings with those in Section 2. From the continuity equation, vertical  
 18 velocity is related to the divergence  $\delta$  by  $\omega = \int_0^p \delta dp$ .

## 19 **Appendix B**

20 Multiplying (28) by  $A_n^*$ , the complex conjugate function of  $A_n$ , we have

21

$$22 \quad A_n^* \sigma \nabla^2 A_n - \lambda_n A_n^* \frac{\partial^2 A_n}{\partial p^2} = 0 \quad (\text{B1})$$



1

2

Also, multiplying the complex conjugate of (28), i.e.

3

4

$$\sigma \nabla^2 A_n^* - \lambda_n^* \frac{\partial^2 A_n^*}{\partial p^2} = 0 \quad (B2)$$

5

6

by  $A_n$  yields

7

8

$$A_n \sigma \nabla^2 A_n^* - \lambda_n^* A_n \frac{\partial^2 A_n^*}{\partial p^2} = 0 \quad (B3)$$

9

10

Notice also that

11

12

$$\lambda_n A_n^* \frac{\partial^2 A_n}{\partial p^2} = \lambda_n \left[ \frac{\partial}{\partial p} \left( A_n^* \frac{\partial A_n}{\partial p} \right) - \left\| \frac{\partial A_n}{\partial p} \right\|^2 \right] \quad (B4a)$$

13

$$\lambda_n^* A_n \frac{\partial^2 A_n^*}{\partial p^2} = \lambda_n^* \left[ \frac{\partial}{\partial p} \left( A_n \frac{\partial A_n^*}{\partial p} \right) - \left\| \frac{\partial A_n}{\partial p} \right\|^2 \right] \quad (B4b)$$

14

and

15

$$A^* \sigma \nabla^2 A = \nabla \cdot (A^* \sigma \nabla A) - \sigma \|\nabla A\|^2 - A^* \nabla \sigma \cdot \nabla A \quad (B5a)$$

16

$$A \sigma \nabla^2 A^* = \nabla \cdot (A \sigma \nabla A^*) - \sigma \|\nabla A\|^2 - A \nabla \sigma \cdot \nabla A^* \quad (B5b)$$

17

18

Integrating (A1.1)+(A1.3) and (A1.1)-(A1.3) over domain  $\Omega$ , we have (30a) and (30b), respectively. Here,

19

$$\int_{\Omega} (\cdot) d\Omega = \iint_S \int_0^{p_s} (\cdot) dp dS; \quad \Omega = S \times [0, p_s] \quad (B6)$$





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3  $S$  is the area of meso-scale system, while  $p_s$  is surface pressure. In the derivation, the following relations are  
 4 employed

$$5 \quad A_n^* \sigma \nabla^2 A_n - A_n \sigma \nabla^2 A_n^* = \nabla \cdot (A_n^* \sigma \nabla A_n - A_n \sigma \nabla A_n^*) + \nabla \sigma \cdot (A_n \nabla A_n^* - A_n^* \nabla A_n) \quad (B7a)$$

6

$$7 \quad A_n^* \sigma \nabla^2 A_n + A_n \sigma \nabla^2 A_n^* = \nabla \cdot (A_n^* \sigma \nabla A_n + A_n \sigma \nabla A_n^*) - 2\sigma \|\nabla A_n\|^2 - \nabla \sigma \cdot \nabla \|A_n\|^2 \\ 8 \quad = \nabla \cdot (A_n^* \sigma \nabla A_n + A_n \sigma \nabla A_n^* - \|A_n\|^2 \nabla \sigma) - 2\sigma \|\nabla A_n\|^2 + \|A_n\|^2 \Delta \sigma \quad (B7b)$$

9 And boundary conditions as below are considered as well

$$10 \quad A_n^* \frac{\partial A_n}{\partial p} \Big|_{p=0, p_s} = 0; \quad A_n \frac{\partial A_n^*}{\partial p} \Big|_{p=0, p_s} = 0 \quad (B8)$$

11

$$12 \quad (A^* \sigma \nabla A + A \sigma \nabla A^* - \|A\|^2 \nabla \sigma) \cdot \hat{n} \Big|_{s \rightarrow \infty} = 0 \quad (B9a)$$

$$12 \quad \sigma (A \nabla A^* - A^* \nabla A) \cdot \hat{n} \Big|_{s \rightarrow \infty} = 0 \quad (B9b)$$

13

## 14 Appendix C

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16 Similarly to the way in Zhao and Gan (2010) for a barotropic model, the Green's function  $G$  in (50) is  
 17 obtained as below. Since  $G$  satisfies

$$17 \quad \frac{\partial^2 G}{\partial t^2} - c_n^2 \nabla^2 G + f^2 G = \delta(\mathbf{r} - \mathbf{r}') \delta(t - t') \quad (C1)$$

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20 Its Fourier transform with respect to  $t$  gives

$$21 \quad \nabla^2 \tilde{G} + \frac{\omega^2 - f^2}{c_n^2} \tilde{G} = -\delta(\mathbf{r} - \mathbf{r}') e^{-i\omega t'} \quad (C2)$$



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Here  $\tilde{G}$  is the Fourier transform of  $G$ . From the Green function of Helmholtz equation, one obtains

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$$\tilde{G}(\mathbf{r}, \mathbf{r}', \omega) = \frac{i}{4} H_0^{(1)}\left(\sqrt{\frac{\omega^2 - f^2}{c_n^2}} |\mathbf{r} - \mathbf{r}'|\right) e^{-i\omega t} \quad (\text{C3})$$

5

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Here  $H_0^{(1)}$  is Hankel function. The inverse Fourier transform of (A2.3) gives the Green's function  $G$  in (50),

7

in which following formulas are utilized in its derivation

8

9

$$F^{-1}[i\pi H_0^{(1)}(a\sqrt{b^2 - \omega^2})] = \frac{\exp(ib\sqrt{t^2 + a^2})}{\sqrt{t^2 + a^2}} \quad (\text{C4a})$$

10

$$F^{-1}[\tilde{A}(\omega)e^{-i\omega\beta}] = A(t - \beta) \quad (\text{C4b})$$

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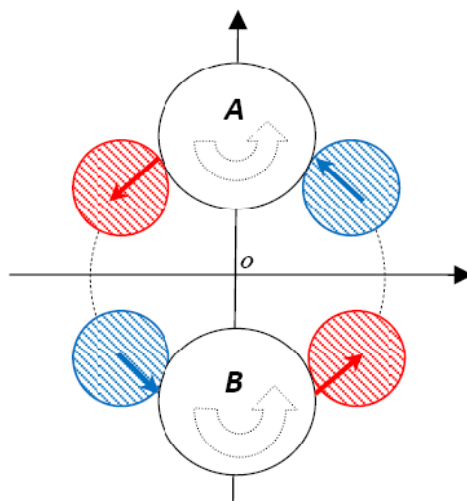
<i>Type of instability</i>	<i>Balanced basic flow</i>	<i>Equation describing instability</i>	<i>Remarks</i>
Static instability	Static state	$\frac{\partial^2 \delta_{pp}}{\partial t^2} + \sigma \nabla^2 \delta + f^2 \delta_{pp} = 0$	$\sigma < 0$
Symmetric instability	Geostrophic flow $U$ ( $x$ -oriented)	$\frac{\partial^2 \delta_{pp}}{\partial t^2} + N^2 \delta_{yy} - 2S^2 \delta_{yp} + F^2 \delta_{pp} = 0$	$N^2 = \sigma$ , $S^2 = fU_p$ , $F^2 = f(f + U_y)$
Kelvin-Helmholtz instability	Parallel flow $U$ ( $x$ -oriented)	$\frac{\partial^2 \delta_{pp}}{\partial t^2} + \sigma \nabla^2 \delta + f^2 \delta_{pp} + U \frac{\partial \delta_{xpp}}{\partial t} + U_p \frac{\partial \delta_{xp}}{\partial t} - f U_p \delta_{yp} = 0$	$U_y = 0$ ; $U_p \neq 0$
Inertia instability	Gradient wind $U$ ( $r$ -oriented)	$\frac{\partial^2 \delta_{pp}}{\partial t^2} + \sigma \nabla^2 \delta + f(f + \zeta_0) \delta_{pp} + \zeta_0 \frac{\partial}{\partial t} \frac{\partial \delta_{pp}}{\partial \theta} = 0$	$U_\theta = \zeta_0 r$ $U_p = 0$

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13 Table I. Types of linear instabilities, corresponding balanced basic flows and equations describing these  
 14 instabilities.



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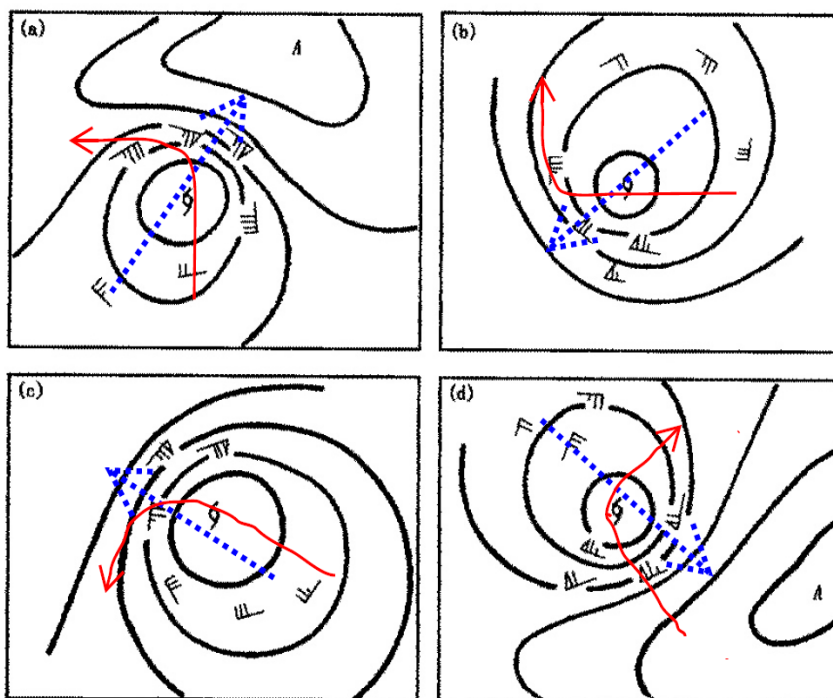
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9 **Figure 1.** Cyclonically orbiting of the two typhoons *A* and *B* about the origin *o* may cause positive  
10 (negative) vorticity advection in front of (behind) each single typhoon, with respect to the directions of  
11 their motions. This distribution of vorticity advection has central antisymmetric structure, i.e. the values of  
12 vorticity advection at  $(x, y)$  and  $(-x, -y)$  are the same, and meanwhile it is also symmetric about two axes. So  
13 vorticity advection appears to be primarily a quadrupole structure.

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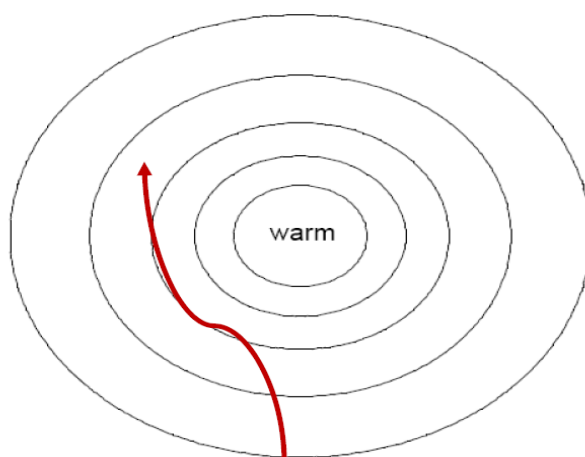
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16 **Figure 2.** The averaged vorticity gradient  $\overline{\nabla\zeta}$  and the turning of typhoon track are marked by arrows in  
17 blue dashed line and red solid line respectively upon the figure of stream fields in Chen et al. (2002 ).

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**Figure 3.** The arrow in red thick solid line represents a typhoon track approaching a warm sea region indicated by the contour lines (dark thin line) of SST.